

# SURFACE ELECTROMYOGRAPHY: DETECTION AND RECORDING

#### Carlo J. De Luca

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#### CONTENTS

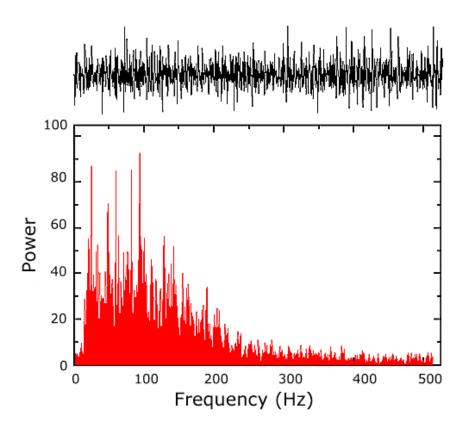
GENERAL CONCERNS	. 2
CHARACTERISTICS OF THE EMG SIGNAL	. 2
CHARACTERISTICS OF THE ELECTRICAL NOISE	. 3
MAXIMIZING THE FIDELITY OF THE EMG SIGNAL	. 3
ELECTRODE AND AMPLIFIER DESIGN	. 4
ELECTRODE GEOMETRY	. 6
THE PARALLEL-BAR ELECTRODE	. 7
EMG ELECTRODE PLACEMENT	. 8
REFERENCE ELECTRODE PLACEMENT	. 9
ELECTRICAL SAFETY CONCERNS	. 9
EMG SIGNAL PROCESSING	. 9
APPLICATIONS OF THE EMG SIGNAL	10

#### **GENERAL CONCERNS**

When detecting and recording the EMG signal, there are two main issues of concern that influence the fidelity of the signal. The first is the signal to noise ratio. That is, the ratio of the energy in the EMG signal to the energy in the noise signal. In general, noise is defined as electrical signals that are not part of the wanted EMG signal. The other is the distortion of the signal, meaning that the relative contribution of any frequency component in the EMG signal should not be altered.

#### CHARACTERISTICS OF THE EMG SIGNAL

It is well established that the amplitude of the EMG signal is stochastic (random) in nature and can be reasonably represented by a Gausian distribution function. The amplitude of the signal can range from 0 to 10 mV (peak-to-peak) or 0 to 1.5 mV (rms). The usable energy of the signal is limited to the 0 to 500 Hz frequency range, with the dominant energy being in the 50-150 Hz range. Usable signals are those with energy above the electrical noise level. An example of the frequency spectrum of the EMG signal is presented in *Figure 1*.



*Figure 1: Frequency spectrum of the EMG signal detected from the Tibialis Anterior muscle during a constant force isometric contraction at 50% of voluntary maximum.* 

#### **CHARACTERISTICS OF THE ELECTRICAL NOISE**

The noise may emanate from various sources such as:

- Inherent noise in the electronics components in the detection and recording equipment All electronics equipment generates electrical noise. This noise has frequency components that range from 0 Hz to several thousand Hz. This noise cannot be eliminated; it can only be reduced by using high quality electronic components, intelligent circuit design and construction techniques.
- Ambient noise This noise originates from sources of electromagnetic radiation, such as radio and television transmission, electrical-power wires, light bulbs, fluorescent lamps, etc. In fact, any electromagnetic device generates and may contribute noise. The surfaces of our bodies are constantly inundated with electric-magnetic radiation and it is virtually impossible to avoid exposure to it on the surface of the earth. The dominant concern for the ambient noise arises from the 60 Hz (or 50 Hz) radiation from power sources. The ambient noise signal may have an amplitude that is one to three orders of magnitude greater than the EMG signal.
- **Motion artifacts** There are two main sources of motion artifact: one from the interface between the detection surface of the electrode and the skin, the other from movement of the cable connecting the electrode to the amplifier. Both of these sources can be essentially reduced by proper design of the electronics circuitry. The electrical signals of both noise sources have most of their energy in the frequency range from 0 to 20 Hz.
- Inherent instability of the signal The amplitude of the EMG signal is quasi-random in nature. The frequency components between 0 and 20 Hz are particularly unstable because they are affected by the quasi-random nature of the firing rate of the motor units which, in most conditions, fire in this frequency region. Because of the unstable nature of these components of the signal, it is advisable to consider them as unwanted noise and remove them from the signal.

#### MAXIMIZING THE FIDELITY OF THE EMG SIGNAL

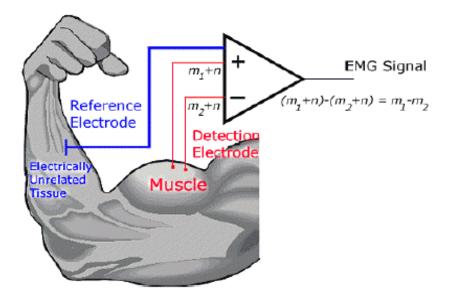
It is desirable to obtain an EMG signal that contains the maximum amount of information from the EMG signal and the minimum amount of contamination from electrical noise. Thus, the maximization of the signal-to-noise ratio should be done with minimal distortion to the EMG signal. Therefore, it is important that any detecting and recording device process the signal linearly. In particular, the signal should not be clipped, that is, the peaks should not be distorted and no unnecessary filtering should be performed.

Because the power line radiation (50 or 60 Hz) is a dominant source of electrical noise, it is tempting to design devices that have a notch-filter at this frequency. Theoretically, this type of filter would only remove the unwanted power line frequency, however, practical implementations also remove portions of the adjacent frequency components. Because the dominant energy of the EMG signal is located in the 50-100 Hz range, the use of notch filters is not advisable when there are alternative methods of dealing with the power line radiation.

#### ELECTRODE AND AMPLIFIER DESIGN

The design of the electrode unit is the most critical aspect of the electronics apparatus which will be used to obtain the signal. The fidelity of the EMG signal detected by the electrode influences all subsequent treatment of the signal. It is very difficult (almost impossible) to improve the fidelity and signal-to-noise ratio of the signal beyond this point. Therefore, it is important to devise an electrode unit that provides minimal distortion and highest signal-to-noise ratio. The following characteristics are important for achieving this requirement.

**Differential amplification** - In order to eliminate the potentially much greater noise signal from power line sources, a differential detecting configuration is employed. The differential amplification technique is shown schematically in *Figure 2*. The premise is simple. The signal is detected at two sites, electronics circuitry subtracts the two signals and then amplifies the difference. As a result, any signal that is "common" to both detection sites will be removed and signals that are different at the two sites will have a "differential" that will be amplified. Any signal that originates far away from the detection sites will appear as a common signal, whereas signals in the immediate vicinity of the detection surfaces will be different and consequently will be amplified. Thus, relatively distant power lines noise signals will be removed and relatively local EMG signals will be amplified. This explanation requires the availability of a highly accurate "subtractor". In practice, even with the wondrous electronics of today, it is very difficult to subtract signals perfectly. The accuracy with which the differential amplifier can subtract the signals is measured by the Common Mode Rejection Ratio (CMRR). A perfect subtractor would have a CMRR of infinity. A CMRR of 32,000 or 90 dB is generally sufficient to suppress extraneous electrical noises. Current technology allows for a CMRR of 120 dB, but there are at least three reasons for not pushing the CMRR to the limit: 1) Such devices are expensive. 2) They are difficult to maintain electrically stable, and 3) the extraneous noise signals may not arrive at the two detection surfaces in phase, and hence they are not common mode signals in the absolute sense.



*Figure 2: A schematic of the differential amplifier configuration. The EMG signal is represented by 'm' and the noise signals by 'n'.* 

- **Input impedance** The source impedance at the junction of the skin and detection surface may range from several thousand ohms to several megohms for dry skin. In order to prevent attenuation and distortion of the detected signal due to the effects of input loading, the input impedance of the differential amplifier should be as large as possible, without causing ancillary complications to the workings of the differential amplifier. Present day electronics devices easily provide input impedances of the order of 1012 ohms in parallel with 5 picofarads. In addition to the magnitude of the input impedance, the balance between the impedances of the two detection sites is also of great importance. This consideration requires careful circuit design.
- Active electrode design The requirement for a high input impedance introduces a problem known as capacitance coupling at the input of the differential amplifier. A small capacitance between the wires leading to the input of the differential amplifier and the power line will introduce a power line noise signal into the amplifier. This phenomenon is similar to that which causes a television signal strength to increase when one places ones hand near the antenna input, but does not touch it. The solution is to place the differential amplifier as close as possible to the detection surfaces of the electrode. This solution has become known as the "active electrode". One other advantage of this configuration is that the output impedance of the differential amplifier can be made to be very low, on the order of 10 ohms. Therefore, any movement of the cable from the output of the electrode will not generate significant or even notable noise signals in the cable which feeds into the subsequent amplifier.
- **Filtering** Even with the above considerations, the EMG signal will be contaminated by some noise. The signal to noise ratio can be increased by judicious filtering between 20-500 Hz with a roll-off of 12 dB/oct. (Strict design characteristics could consider 400 Hz as the upper bandwidth cut-off. The 500 Hz value allows for a safety margin in the design of the circuitry.) This filtering is generally accomplished at the amplifier stage located outside the active electrode.
- Electrode stability When an electrode is placed on the skin, the detection surfaces come in contact with the electrolytes in the skin. A chemical reaction takes place which requires some time to stabilize, typically in the order of a few seconds if the electrode is correctly designed. But, more importantly, the chemical reaction should remain stable during the recording session and should not change significantly if the electrical characteristics of the skin change from sweating or humidity changes.
- **Preferred method of use** Given the high performance and small size of modern day electronics, it is possible to design active electrodes that satisfy the above requirements without requiring any abrasive skin preparation and removal of hair.

#### **ELECTRODE GEOMETRY**

Throughout the history of electromyography, the shape and the layout of the detection surface of the electrode have not received much attention. Most likely because past users of electromyography have been interested only in the qualitative aspects of the EMG signal. The advent of new processing techniques for extracting quantitative information from the EMG signal requires greater focus on the configuration of the electrode. The major (but not all) points to consider are:

- 1.) the signal to noise ratio of the detected signal,
- 2.) the bandwidth of the signal,
- 3.) the muscle sample size, and
- 4.) the susceptibility to crosstalk.
- Signal-to-noise ratio The signal-to-noise ratio is a function of complicated interactions between the electrolytes in the skin and the metal of the detection surfaces of the electrode. This is an involved subject that is beyond the scope of this short treatise. Suffice it to say that there are several approaches for reducing the noise, such as using large surface areas for the detection surfaces, employing conductive electrolytes to improve the contact with the skin, and removing dead (less conductive) dermis from the surface of the skin. Through trial and error we have found that detection surfaces made of pure (>99.5%) silver in the form of bars 1 cm in length and 1 mm in width provide a sufficiently good medium for the detection surface.

The amplitude of the EMG signal is directly proportional to the distance between the detection surfaces. Hence, this distance should be maximized. But, increasing this distance introduces undesirable characteristics to the electrode design. As the electrode becomes larger, it becomes unwieldy and cannot be used to detect EMG signals from relatively small (in width as well as in length) muscles such as those found in the hand, forearm and the leg. Additionally, as the distance increases the filtering characteristics of the differential amplification decreases in bandwidth. (Explanation of this esoteric point may be found in Chapter 2 of Muscles Alive (1985) by Basmajian and De Luca.) Thus, a compromise is necessary. We have found by calculations and by heuristics that an inter-detection surface spacing of 1 cm provides an acceptable compromise.

- **Bandwith** -The bandwidth of the EMG signal is affected by the inter-detection surface spacing and the conduction velocity of the action potentials along the muscle fibers. The differential configuration possesses a spatial filtering feature that can be expresses as a bandpass filter in the spectral frequency region of the EMG signal. Again see Muscles Alive (1985) pp. 46-50 for details. For an average conduction velocity of 4.0 m/s and an inter-detection surface distance of 1.0 cm, the pass frequency is 200 Hz and the null point is at 400 Hz. This bandwidth captures the full frequency spectrum of the EMG signal and suppresses noise at higher frequencies.
- **Muscle sample size** The muscle sample size need not be large because the muscle fibers of motor units are distributed throughout most of the muscle cross-section. Therefore, it is not necessary to cover a large portion of the muscle with the detection surface of the electrode to obtain a representative sample of the EMG signal for a particular set of active motor units.
- **Cross-talk susceptibility** The susceptibility to cross-talk is an often overlooked design aspect of EMG electrodes. The greater the width and length of the detection surfaces and the greater the interdetection surface distance the closer the electrode will be to adjacent muscles. Thus, larger electrodes are more susceptible to detecting signals from adjacent (lateral and below) muscles. In situations where this issue is of concern, it is advisable to reduce the size of the electrode.

## THE PARALLEL-BAR ELECTRODE

From the above discussion, it is apparent that the design of a general-purpose electrode can only be realized by making compromises on the dimensions and configuration of the detection surfaces and the interdetection surface distance. Our experience has led us to use parallel bars (1cm long and 1mm wide) spaces 1 cm apart as shown in the following figure.

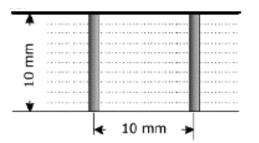


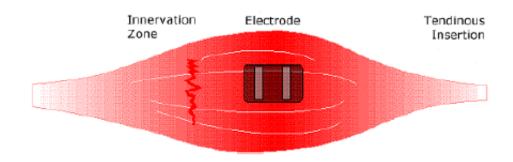
Figure 3: Schematic representation of bar and circular configurations for electrodes.

In addition to satisfying most of the above requirements this configuration also has some practical advantages:

- 1. It can be constructed so that it is sufficiently small and lightweight as to not be obtrusive to the subject.
- 2. The spacing of 1 cm between the detection surfaces is sufficiently large so as not to provide a prohibitive electrical shorting path when the skin sweats.

#### EMG ELECTRODE PLACEMENT

• Location and orientation of the electrode - The electrode should be placed between a motor point and the tendon insertion or between two motor points, and along the longitudinal midline of the muscle. The longitudinal axis of the electrode (which passes through both detection surfaces) should be aligned parallel to the length of the muscle fibers. *Figure 4* provides a schematic representation of the preferred electrode location.



*Figure 4: The preferred electrode location is between the motor point (or innervation zone) and the tendinous insertion, with the detection surfaces arranged so that they intersect as many muscle fibers as possible.* 

- **NOT on or near the tendon of the muscle** As the muscle fibers approach the fibers of the tendon, the muscle fibers become thinner and fewer in number, reducing the amplitude of the EMG signal. Also in this region the physical dimension of the muscle is considerably reduced rendering it difficult to properly locate the electrode, and making the detection of the signal susceptible to crosstalk because of the likely proximity of agonistic muscles.
- NOT on the motor point During the past one-half century it has been taught that for the purpose of detecting a surface EMG signal the electrode should be located on a motor point of the muscle. The motor point is that point on the muscle where the introduction of minimal electrical current causes a perceptible twitch of the surface muscle fibers. This point usually, but not always, corresponds to that part of the innervation zone in the muscle having the greatest neural density, depending on the anisotropy of the muscle in this region. Presumably, the motor points have been used as landmarks because they were identifiable and provided a fixed anatomical landmark. Unfortunately from the point of view of signal stability, a motor point provides the worst location for detecting an EMG signal. In the region of a motor point, the action potentials travel caudally and rostrally along the muscle fibers, thus the positive and negative phases of the action potentials (detected by the differential configuration) will add and subtract with minor phase differences causing the resulting EMG signal to have higher frequency components. In the time domain, the signal appears as more jagged and with more sharp peaks. The loss of stability occurs from the fact that a minor displacement (0.1 mm) will affect in an unpredictable fashion the amount of change in the frequency characteristics of the signal.

A note of caution about the motor points and innervation zones. Most muscles have multiple innervation zones throughout the muscle. They can be identified by applying electrical stimulation to the skin above the surface of the muscle or by other more technically complicated surface mapping techniques. If neither procedure is convenient, then place the electrode in the middle of the muscle between the origin and insertion point.

- **NOT at the outside edges of the muscle** In this region, the electrode is susceptible to detecting crosstalk signals from adjacent muscles. It is good practice to avoid this situation. For some applications, crosstalk signals may be undesirable.
- Orientation of the electrode with respect to the muscle fibers The longitudinal axis of the electrode (which passes through both detection surfaces) should be aligned parallel to the length of the muscle fibers. When so arranged, both detection surfaces will intersect most of the same muscle fibers. Hence, the spectral characteristics of the EMG signal will reflect the properties of a fixed set of muscle fibers in the region of the electrode. Also, the frequency spectrum of the EMG signal will be independent of any trigonometric factor that would provide an erroneous estimate of the conduction velocity. The resultant value of the conduction velocity affects the EMG signal by altering the temporal characteristics of the EMG signal, and consequently its frequency spectrum.

### **REFERENCE ELECTRODE PLACEMENT**

The reference electrode (at times called the ground electrode) is necessary for providing a common reference to the differential input of the preamplifier in the electrode. For this purpose, the reference electrode should be placed as far away as possible and on electrically neutral tissue (say over a bony prominence). Often this arrangement is inconvenient because the separation of the detecting electrode and reference electrode leads requires two wires between the electrodes and the amplifier.

It is imperative that the reference electrode make very good electrical contact with the skin. For this reason, the electrode should be large (2 cm x 2 cm). If smaller, the material must be highly conductive and should have strong adhesive properties that will secure it to the skin with considerable mechanical stability. Electrically conductive gels are particularly good for this purpose. Often, power line interference noise may be reduced and eliminated by judicious placement of the ground electrode.

## ELECTRICAL SAFETY CONCERNS

The failure of any electrical instrumentation making direct or indirect galvanic contact with the skin can cause a potentially harmful fault current to pass through the skin of the subject. This concern is less relevant in devices that are powered exclusively by low voltage (3-15 V) batteries. To ensure safety, the subject should be electrically isolated from any electrical connection (to the power line or ground) associated with the power source. This isolation is generally achieved in one of two ways: either through the use of optical isolators or through the use of isolation transformers. Both approaches are satisfactory, but both require careful consideration for not distorting the EMG signal. This is especially true when a transformer is used.

This isolation provides the added benefit of reducing the amount of radiated power line noise at the electrode detection surfaces.

#### **EMG SIGNAL PROCESSING**

For several decades it has been commonly accepted that the preferred manner for processing the EMG signal was to calculate the Integrated Rectified signal. This was done by rectifying (rendering the signal to have excursions of one polarity) the EMG signal, integrating the signal over a specified interval of time and subsequently forming a time series of the integrated values. This approach became widespread and it was possible to make these calculations somewhat accurately and inexpensively with the limited electronics technology of earlier decades. The advances made in electronics devices during the past decades have made it possible to conveniently and accurately calculate the root-mean-squared (rms) and the average rectified (avr) value of the EMG signal. The avr value is similar to the integrated rectified value, if the calculations are made correctly and accurately. Both these variables provide a measurement of the area under the signal but do not have a specific physical meaning. On the other hand, the rms value is a measure of the power of the signal, thus it has a clear physical meaning. For this reason, the rms value ispreferred for most applications.

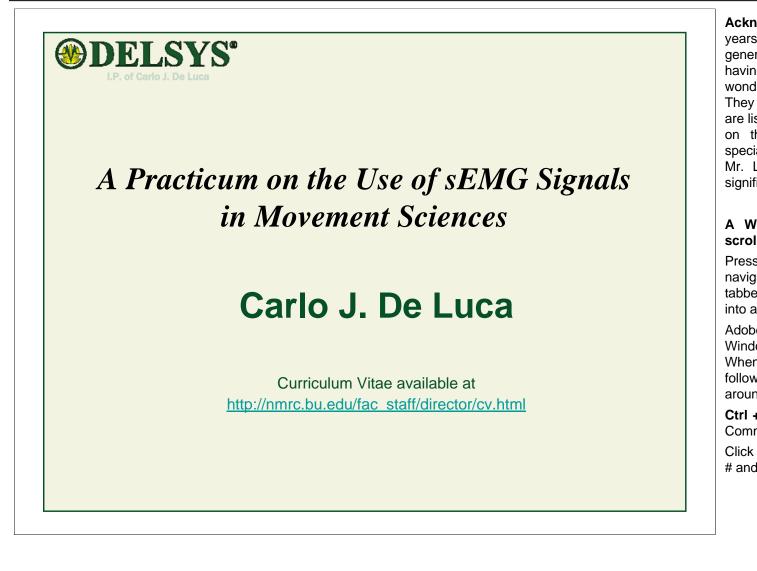
#### **APPLICATIONS OF THE EMG SIGNAL**

Currently there are three common applications of the EMG signal. They are:

- To determine the activation timing of the muscle; that is, when the excitation to the muscle begins and ends
- To estimate the force produced by the muscle.
- To obtain an index of the rate at which a muscle fatigues through the analysis of the frequency spectrum of the signal.

In the not so distant future, we can expect applications in the assessment of neurological diseases which affect the fiber typing or the fiber cross-sectional area of the muscle.

The relationship between the force produced by the muscle and the amplitude of the EMG signal requires further description. During the past five decades, the scientific literature has promulgated an apparent controversy on this issue. Some reports describe a relatively linear relationship, whereas others describe a relative non-linear relationship, with the amplitude of the EMG signal increasing greater than the force. In fact, both positions are correct and the controversy is artificial. It is now known that in small muscles where the firing rate of the motor units has a greater dynamic range and motor unit recruitment is limited to the lower end of the force range, the relationship is relatively linear. Whereas, in larger muscles where motor unit recruitment continues into the upper end of the force range and the firing rate has a lower dynamic range, the relationship is relatively non-linear.



Acknowledgement – Throughout the many years over which this material has been generated, I have had the good fortune of having close collaborations with many wonderful research colleagues and students. They are too many to mention here and some are listed in the cited publications which appear on the slides. Among them, two deserve special mention: Professor Serge H Roy and Mr. L Donald Gilmore. They have made a significant part of this work possible.

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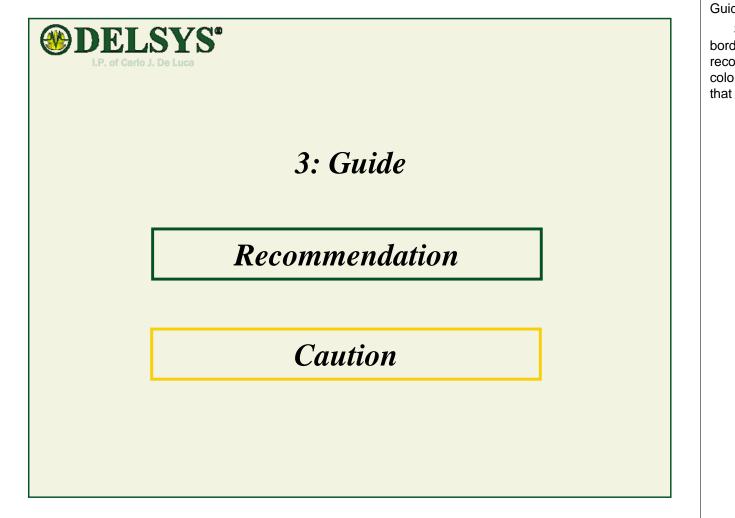
Press F6 on the key board to focus on the navigation pane of Adobe. Within each of the tabbed palettes, lists of objects are organized into a tree structure.

Adobe Acrobat 5.0 follows the standard Windows keyboard behaviors for tree views. When the focus is on the navigation pane, the following keystrokes will help you move around:

**Ctrl + Tab** to access Bookmarks, Thumbnails, Comments, and Signature palettes.

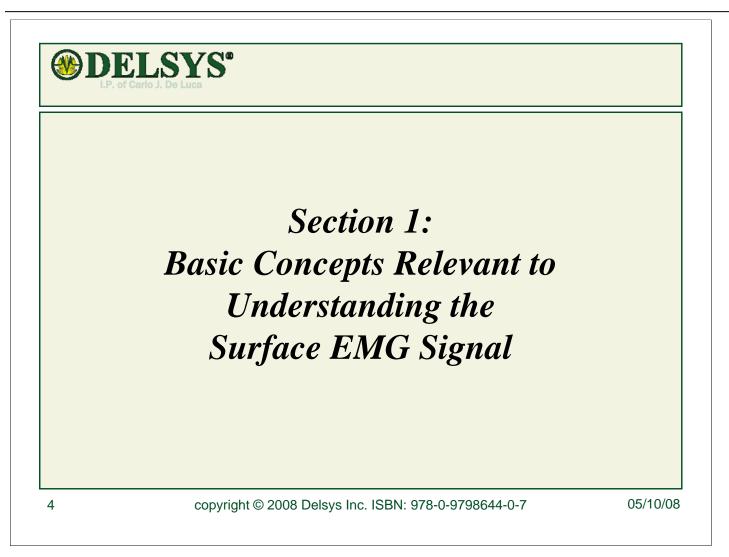
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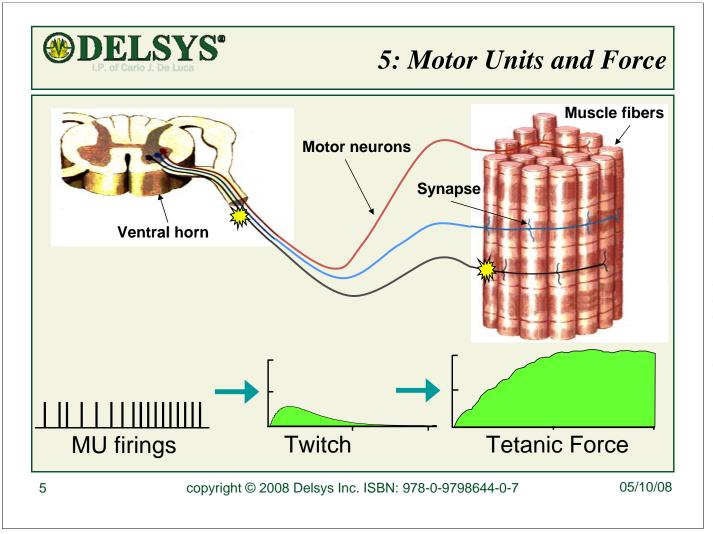
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2:	"Electromyography is too easy to use and consequently too easy to abuse"
<u>De</u>	<u>Luca CJ, The Use of Surface Electromyography in Biomechanics,</u> <u>J. Applied Biomechanics, 13: 135-163, 1997</u>



Guide to slide titles:

Slides with a heading or title without a border are informational, green ones contain recommendations; whereas those with the color yellow describe conditions and issues that should be handled with caution.



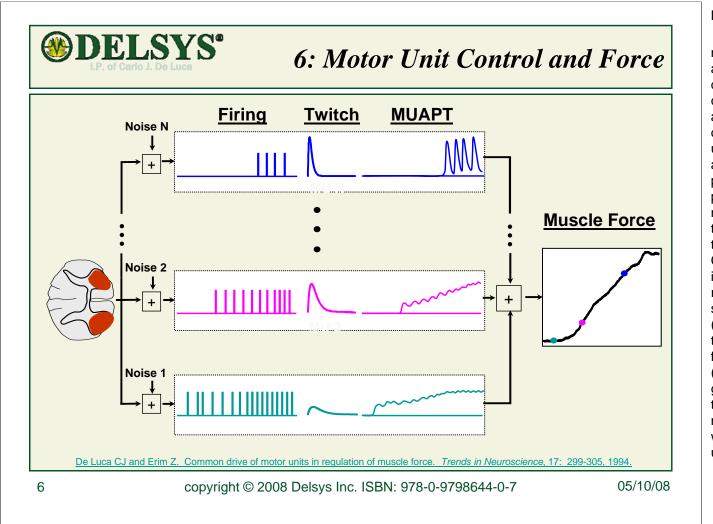


#### Motor Units and Force:

Skeletal muscles are composed of individual muscle fibers that contract when stimulated by a motoneuron. Motoneurons originate in the ventral horn of the spinal cord and consist of a cell body, dendrites (not shown) and an axon. The axon projects to a muscle where it branches, forming synapses with muscle fibers.

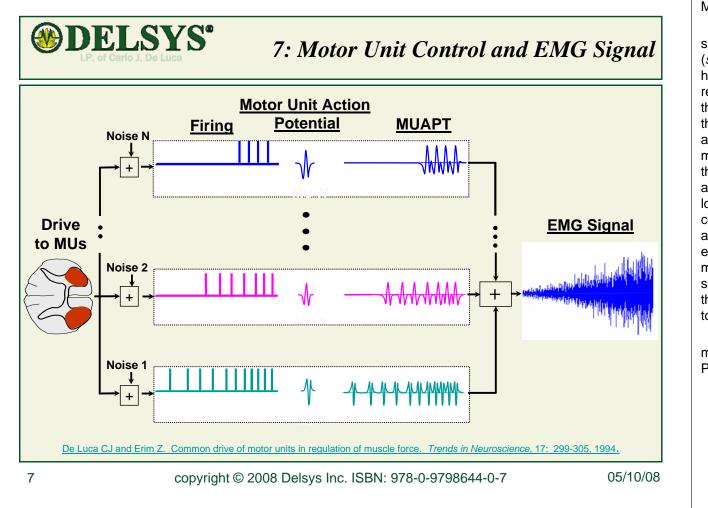
A motor unit is the smallest functional subdivision of a muscle. It consists of the motoneuron, its axon and all the muscle fibers that are innervated by its branches. When motor units are activated, the corresponding muscle fibers contract.

Each firing of a motoneuron produces a force twitch in its motor unit. When force twitches occur in close enough succession they superimpose, producing a tetanic (sustained) force. This sustained force is the mechanism which moves our limbs, enables us to breathe, circulates our blood, and enables us to interact with our environment.



Motor Unit Control and Force:

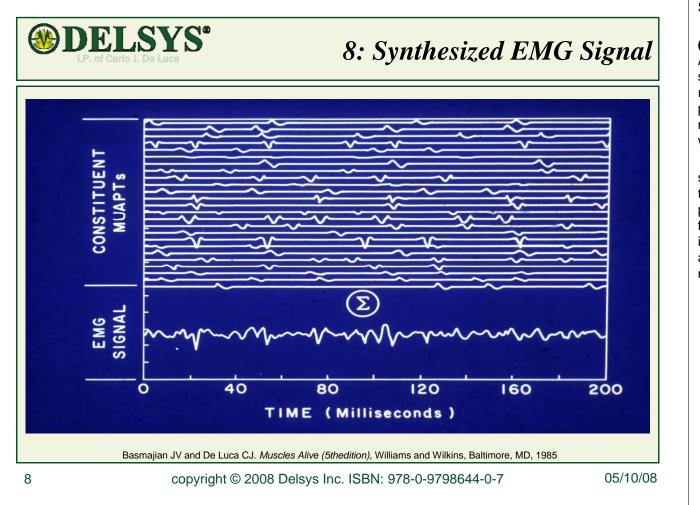
The force output of the muscle is modulated by the recruitment of motor units and the regulation of their firing rates. The diagram presents physiologically correct concepts that relate the excitation at the anterior horn of the spinal cord to the force output of the muscle. Consider a set of motor units (1, ..., n). Each motor unit is activated by a Common Drive (see cited reference) that provides a net excitation to the motoneuron pool in the anterior horn. However, each motoneuron has a noise component (noise N) that consists of background neural activity from the Peripheral Nervous System and from the Central Nervous System. As the excitation increases, motor units are progressively recruited and all the active motor units simultaneously increase their firing rates (mediated by common drive). In this fashion the earlier recruited motor units have greater firing rates than later recruited motor units. (Note that the firing rate of motor unit #1 is greater than MU #2 and MU #n.). Also note that in the above example the earlier-recruited motor units (slow twitch) tend to tetanize, whereas the later-recruited (fast twitch) motor units do not.



Motor Unit Control and EMG Signal:

This figure demonstrates how the EMG signal is generated while the Common Drive (see cited reference) excitation to the anterior horn cell increases. The relationship between recruitment and firing rates is similar to that in the previous companion diagram. Note that as the excitation increases, additional motor units are recruited and the firing rates of all active motor units increases simultaneously. Note that the higher threshold motor units have action potentials of higher amplitude and fire at lower firing rates. Additionally, in sustained contractions at high force levels, the accumulating effects of fatigue may cause the excitation to fluctuate about a set value, then motor units of relatively high amplitudes are sequentially recruited and derecruited causing the variance of the EMG signal (and the force) to increase.

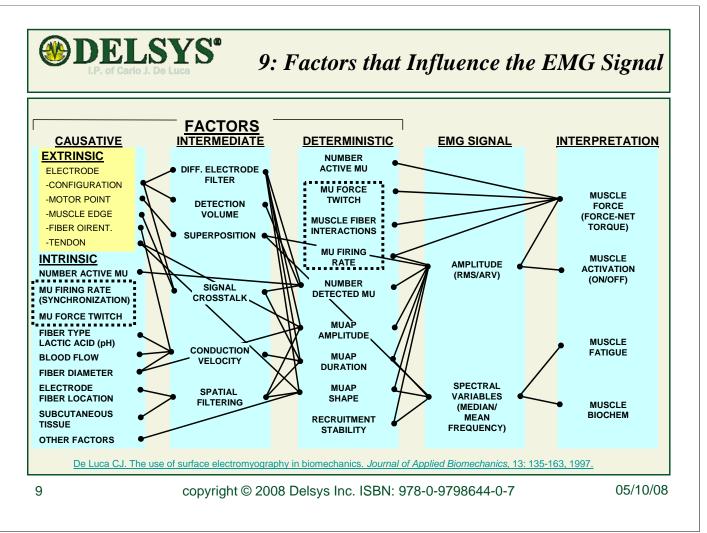
The time sequence of the firings of one motor unit is referred to as a Motor Unit Action Potential Train (**MUAPT**).



#### Synthesized sEMG Signal:

An expanded version of the **surface EMG** (**sEMG**) signal consisting of 25 Motor Unit Action Potential Trains (MUAPT). These are synthesized signals with shapes that closely represent the characteristics of real action potentials. The signal at the bottom is the mathematical sum of all the action potentials which appear in the time sequences above.

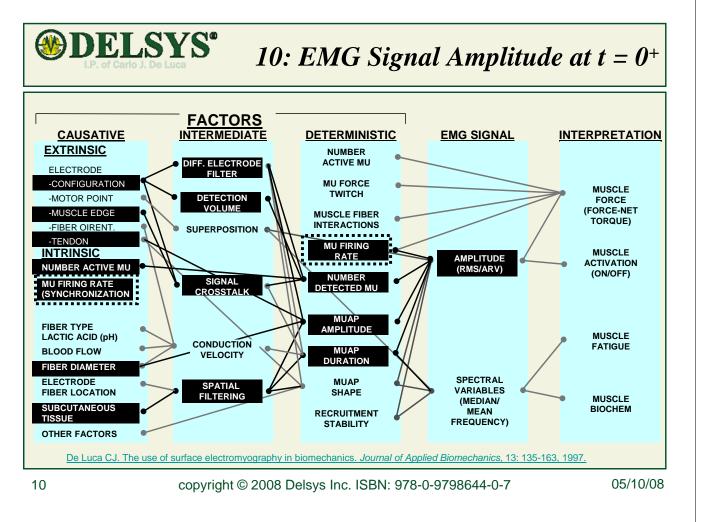
The signal at the bottom is what the sensor sees and the roster above it is the code sent by the CNS that is seen by the muscle fibers. The purpose of EMG signal decomposition is to find, from the signal recorded by the sensor, individual MUAPTs. Being able to do this allows a closer investigation of the control mechanisms governing motor activity.



Factors that Influence the EMG Signal:

Schematic diagram of the factors that affect the EMG signal. The arrangement of factors is designed to demonstrate the flow of influences and interactions among the factors, as well as the complexity of their interaction. The section highlighted in yellow (the extrinsic factors) refers to the sensor design and the manner used to attach the sensor on the skin. These are factors that can be controlled by the sensor manufacturer and sensor user. How and where one locates the sensor on the skin above the muscle has dramatic effect on the signal quality. This topic will be discussed in greater detail in Chapter 3. The intrinsic factors as well as the remaining groups of factors refer to anatomical, physiological, and electrical properties that are not controllable by the user, but must be taken into account when interpreting sEMG results.

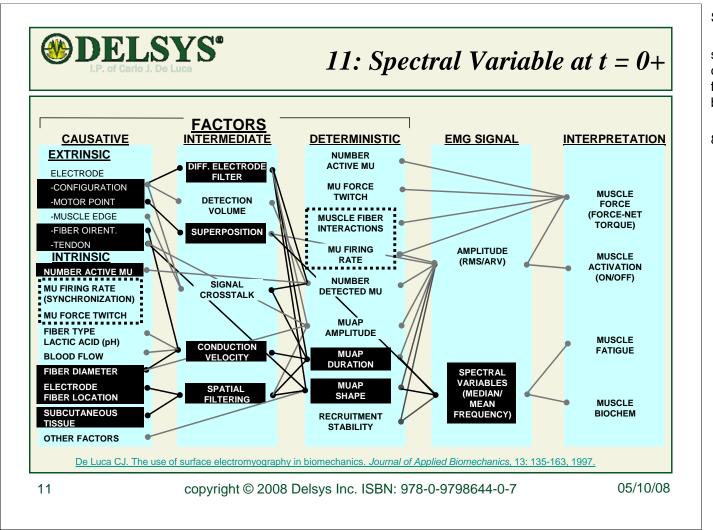
For additional details explaining the remainder of the diagram please refer to the cited reference.



EMG Signal Amplitude at t=0+:

The segments highlighted in black show the interrelationship of factors affecting the EMG signal amplitude at the beginning of a contraction ( $t=0^+$ ), that is when no fatigue is present. Factors which are active at this stage of contraction are shown. The time-dependent (fatigue influencing) factors that would be influential during a sustained contraction are not shown.

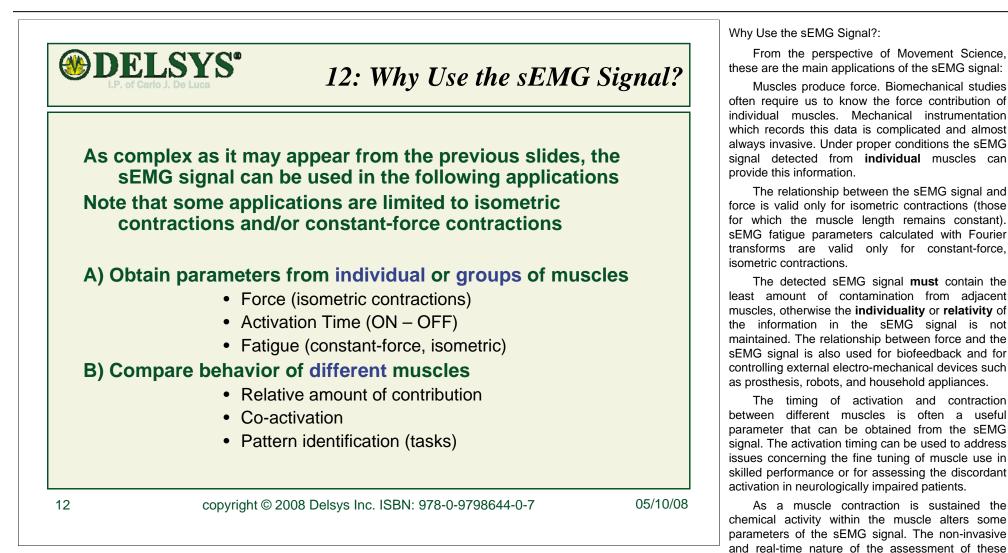
For further explanation about the remainder of the diagram please refer to the cited reference.



Spectral Variable at t=0+:

Factors that influence the frequency spectrum of the sEMG signal at the beginning of a contraction  $(t=0^+)$ , when the influence of fatigue is not present, are shown highlighted in black.

For more on muscle fatigue, skip to slide 87.



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parameters makes the signal useful in some

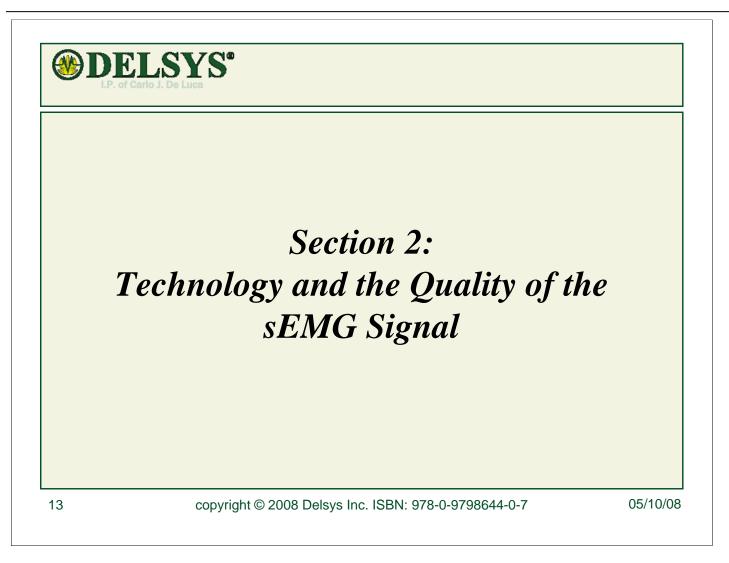
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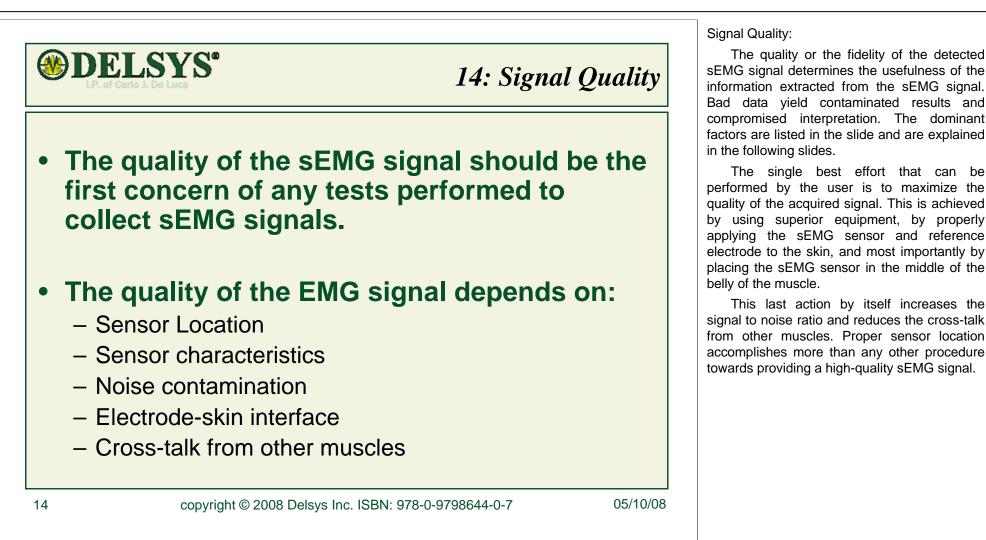
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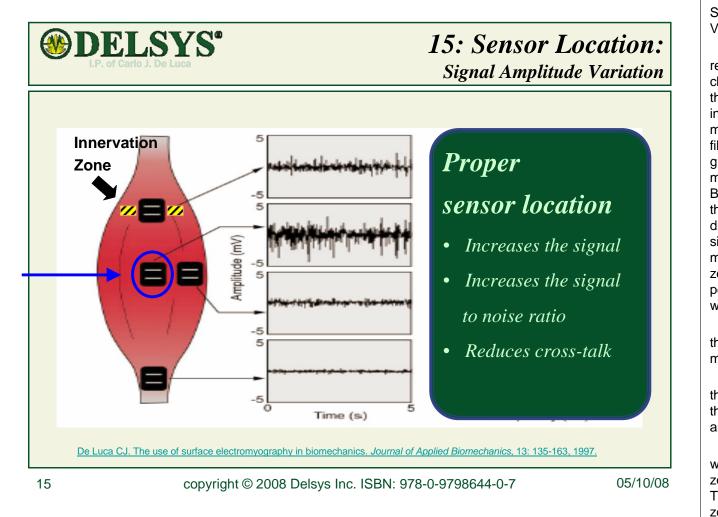
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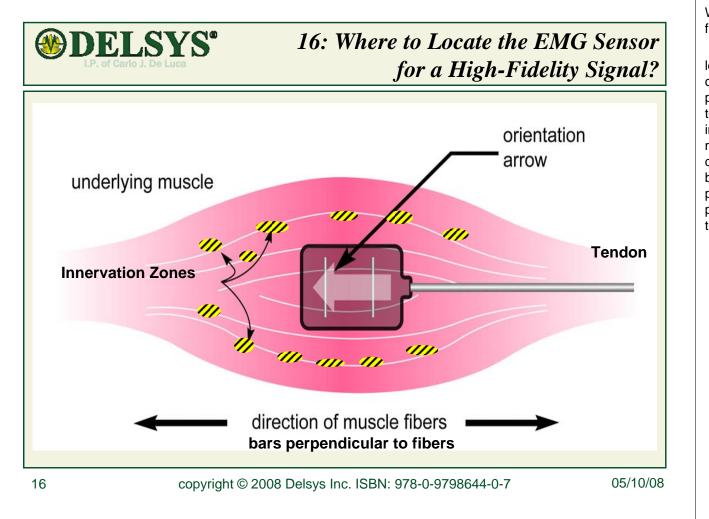
Sensor Location and Signal Amplitude Variation:

The location of the sensor on the muscle renders dramatically different sEMG signal characteristics. Note that locating the sensor in the proximity of the tendon origin, the innervation zone, and the perimeters of the muscle yields lower amplitude signals. The fibers in the middle of the muscle have a greater diameter than those at the edges of the muscle or near the origin of the tendons. Because the amplitude of action potential from the muscle fibers is proportional to the diameter of the fiber, the amplitude of the EMG signal will be greater in the middle of the muscle. A sensor located on the innervation zone will detect the cancellation of the action potentials traveling in opposite direction, and will generally have a lower amplitude.

The preferred location is away from all these boundaries, towards the middle of the muscle surface.

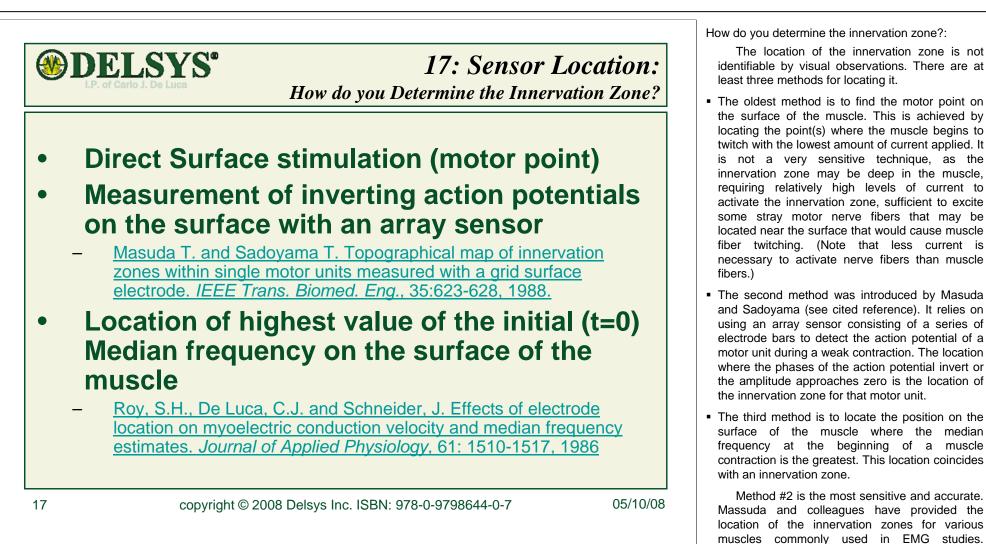
The location of the sensor on the muscle is the single most important factor for obtaining the best signal to noise ratio with the least amount of cross-talk.

Means for locating the innervation zone, as well as known locations of the innervation zones on some muscles, are discussed later. The reported localizations of the innervation zones is in the periphery of the muscle.



Where to locate the EMG sensor for a high-fidelity signal?:

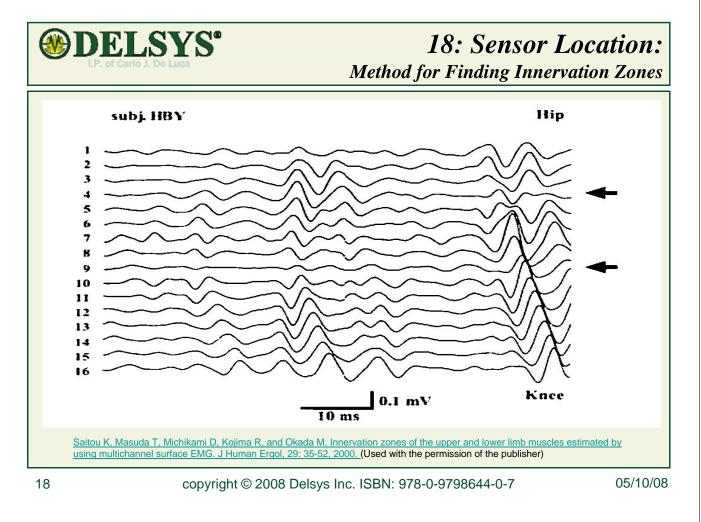
This cartoon indicates the preferred location for placing the sensor -- in the middle of the muscle surface and as far away as possible from the innervation zones and tendon origins. The small yellow striped areas indicate the innervation zones which in large muscles are located around the periphery, as discussed earlier. For better signal quality, the bars of the sensors should be aligned perpendicularly to the muscles fibers when possible. Admittedly, in multi-pennate muscles, this alignment is not possible.



- The location of the innervation zone is not identifiable from visual observations.
- There are at least three ways to calculate it.

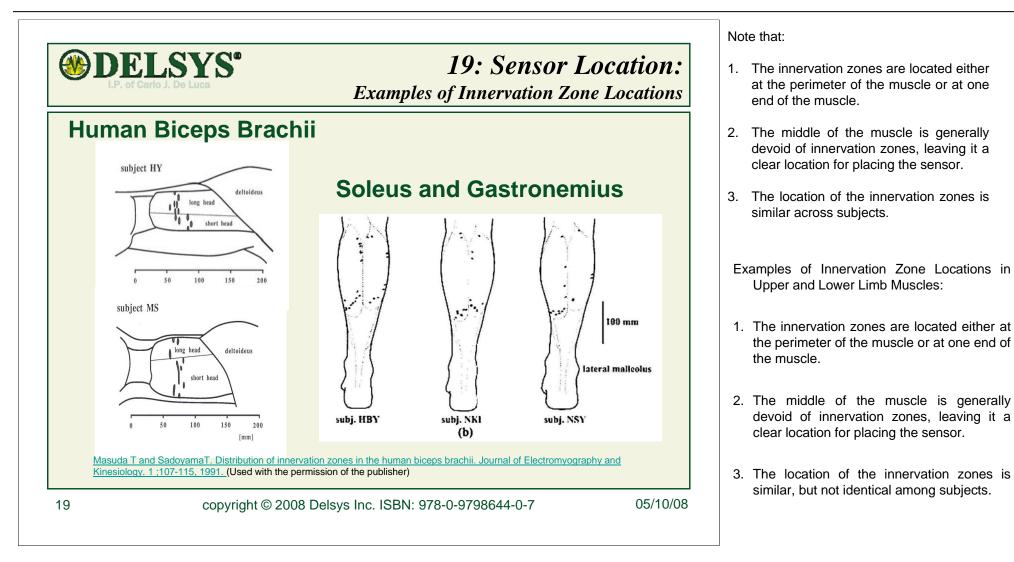
copyright © 2008 Delsys Inc. ISBN: 978-0-9798644-0-7

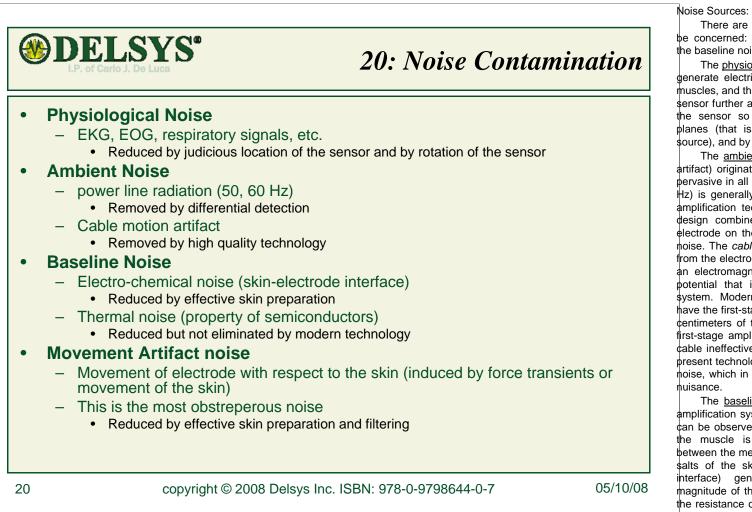
Examples are shown in the next 2 slides.



Method for Determining the Proximity of the Innervation Zone (from Masuda and Sadoyama):

- A linear sensor array of 16 electrodes is placed on the skin above a muscle. A mild contraction is made, sufficient to generate motor unit action potentials that can be visibly identified. The figure shows the time course of three motor unit action potentials
- 2. The action potential travels in both directions from the neuromuscular junctions that constitute the innervation zone. Thus when differential recordings are made between adjacent electrodes, the pair on top of, or in the near proximity of, the neuromuscular junction will detect the lowest amplitude action potential. (If the neuromuscular junction is located precisely between two electrodes and the tissue between the muscle fiber and the electrodes is isotropic, then the amplitude will be zero.)
- 3. The two arrows in the figure indicate the location where the amplitude of two different action potentials is the smallest, indicating the proximity of the innervation zone.





The ambient noise and the baseline noise can be substantially reduced to the level that they are not significant contaminants by using well designed modern technology, by effective preparation of the skin below the sEMG sensor, and by using effective reference electrodes.

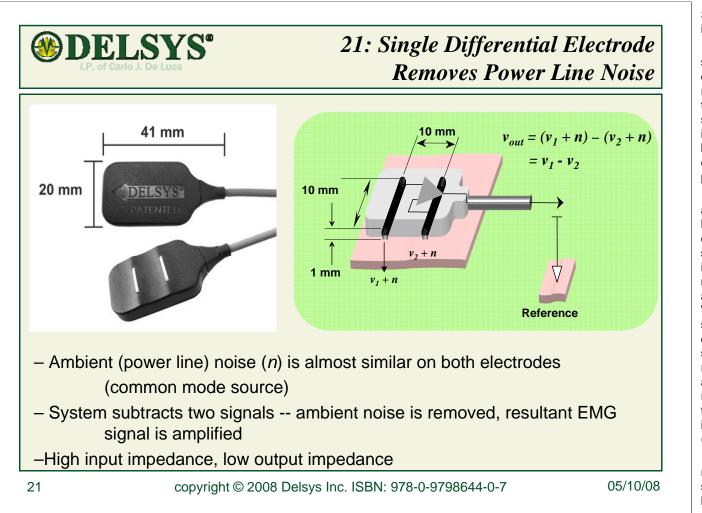
The movement artifact noise also originates at the electrode-skin interface. This noise is the most obstreperous and requires the most attention. There are two common sources. One occurs when a muscle contracts and relaxes causing the length and cross-section to change. This volumetric morphing stretches and relaxes the skin which alters the electro-chemical balance of the two skin-electrode interfaces causing a time-varying voltage across the two electrodes. The other, often much more significant, source occurs when a force impulse originating within the muscle, as in the case of a jerk movement, or from outside the limb, as in the case of a heel-strike while walking, is transmitted to the electrodes. This phenomenon is amplified considerably by the presence of hydrophilic gel that is at times placed between the electrode and the skin [Roy et al., 2007]. It is difficult to reduce and almost impossible to eliminate. A good electrode-skin preparation and appropriate filtering are helpful.

There are several sources of noise with which we must be concerned: The physiological noise, the ambient noise, the baseline noise and the movement artifact noise.

The <u>physiological noise</u> originates from other tissues that generate electrical signals, such as EKG, EOG, respiratory muscles, and the like. It can be reduced by location the sEMG sensor further away from the source of the noise, by rotating the sensor so that the electrodes align on equipotential planes (that is: both electrodes are equidistant from the source), and by some filtering.

The ambient noise (power line noise and cable motion artifact) originates from the electromagnetic radiation that is pervasive in all environments. The power line noise (50 or 60 Hz) is generally not a concern because modern differential amplification technology (see next slide) and proper circuit design combined with judicious location of the reference electrode on the subject can virtually eliminate this ambient hoise. The cable motion artifact originates when the cable(s) from the electrodes or sensor to the amplifier moves and cuts an electromagnetic field in the environment to generate a potential that is subsequently amplified by the recording system. Modern EMG technology now uses sensors that have the first-stage of amplification located on-board or within centimeters of the site of the electrodes. The output of the first-stage amplification has a low-impedance, rendering the cable ineffective in generating a cable motion artifact. Thus, present technology virtually eliminates the first two sources of noise, which in previous decades were a difficult-to-deal-with

The baseline noise originates in the electronics of the amplification system and at the skin-electrode interface. It is can be observed when a sensor is attached to the skin and the muscle is completely relaxed. The ionic exchange between the metal in the electrode and the electrolytes in the salts of the skin (also known as the electrolyte-electrode interface) generates an electro-chemical noise. The magnitude of this noise is proportional to the square root of the resistance of the electrode surface [Huigen et al., 2002]. Thus, it can be reduced by increasing the electrode area and by cleaning the electrode surface, but it cannot be eliminated. The thermal-noise is generated by the first stage of the amplifiers and is due to a physical property of the semiconductors. It also cannot be eliminated. Both noises are referred to as 1/f noises, with the amplitude of the frequency spectrum greatest at 0 Hz and continuously decreasing with increasing frequencies [Huigen et al., 2002]. According to Fernandez and Pallas-Areny [2000] the electrochemical noise is generally greater than the thermal noise.



Definition - The electrode is the metallic detection surface that exchanges ions with the salts in the skin. The sensor is the complete unit that provides the sEMG signal.

The sensor used to detect the sEMG signal is the most important component of the recording system. The fidelity of the signal obtained from the sensor determines the quality of the signal that is provided by the recording system. The remainder of the system can only worsen the quality of the signal. Because the sEMG signal originating in the muscle is much smaller than the ambient electrical signals that originate from surrounding sources, it is strongly recommended (insisted) that the sensor detect "differential" signals.

Single Differential Electrode with low output impedance Removes Ambient Noise:

As may be seen in the green panel, each sensor has two electrodes which detect two different potentials ( $v_1$  and  $v_2$ , which are represented in the figure as voltages) with respect to a reference located some distance from the sEMG sensor. These potentials are caused by the ionic currents that travel along the muscle fibers below the electrodes. Both potentials are contaminated by the noise sources described in the previous slide.

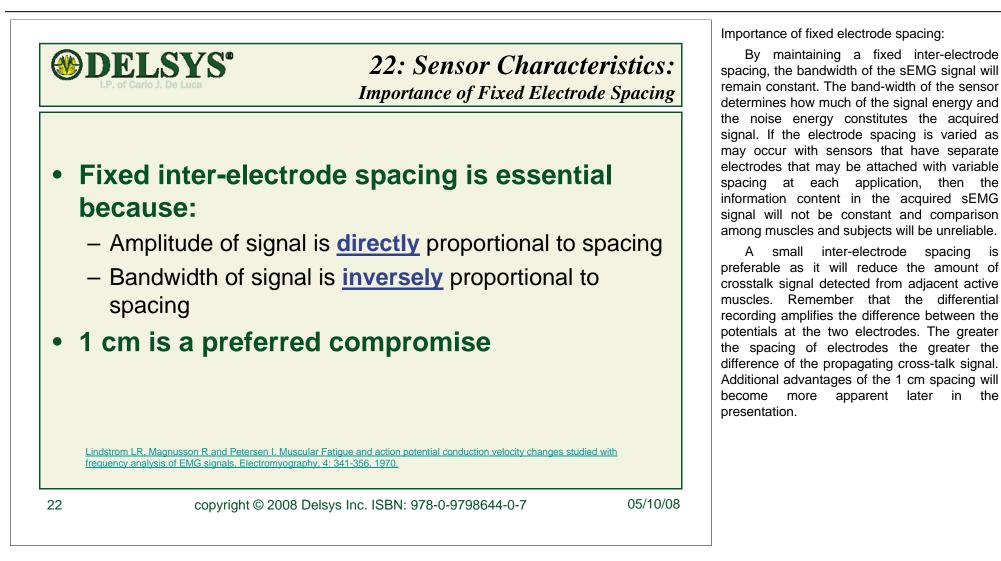
Ambient noise (n) that originated much further away (such as 50 or 60 Hz power line radiation and higher frequency radiation from electronics communication systems, such as radio stations, TV stations, etc.) from the sensors than the interelectrode distance will arrive at the electrodes nearly at the same time, or "in phase". These noises are also known as common - mode signals. Whereas, because the EMG signal travels at speeds of only 2.5 to 5 m/s the two sensors "see" different potentials due to muscle activity. Thus, by subtracting the two potentials, the ambient noise is removed and the difference  $(v_1 - v_2)$  is detected as an sEMG signal. This "difference" potential is the result of "differential" detection. The effectiveness of the circuitry to eliminate the common-mode signals is measured by the Common-mode rejection ration (CMRR).

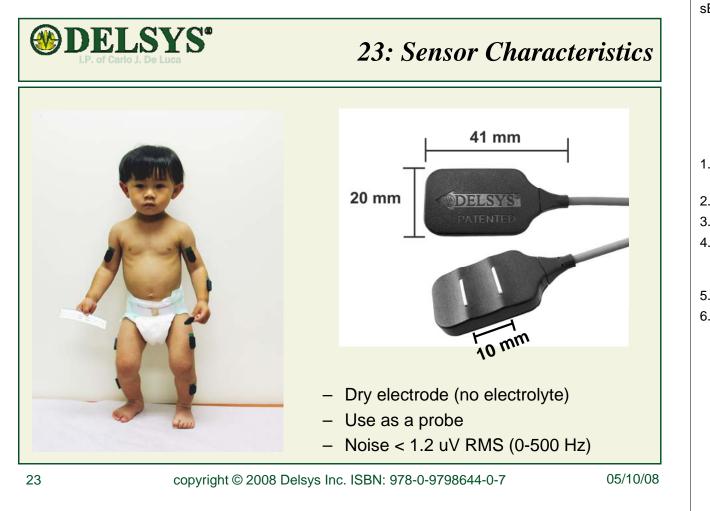
Note that differential amplification will not remove noise contributions from other noise sources such as the EKG, which are local events like the sEMG signal.

FOR MORE INFORMATION ON SENSORS go to <u>Appendix A "sEMG Sensor Factors" located at</u> <u>the end of the practicum</u>.

For more information on the Delsys DE 2.1 sensor go to

http://www.delsys.com/Products/EMGSensors.html





sEMG sensor characteristics:

The Delsys DE 2.1 parallel bar differential sEMG sensor is presented in the slide. For additional information go to http://www.delsys.com/Products/EMGSensors.html

In addition to the electrical characteristics of the sensor, the design of the sensor should address other practical factors such as:

- 1. Effectiveness of the electrical contact between the electrode and the skin
- 2. Facility of attaching the sensor to the skin
- 3. Durability of the adhesion to the skin
- 4. Insensitivity of the electrical and mechanical performance to the presence of sweat.
- 5. Insensitivity to movement artifact
- 6. Ease of use on small muscles



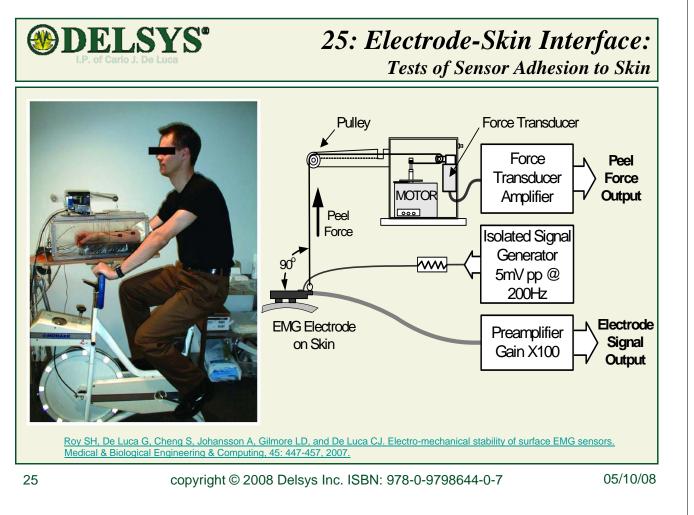
Use of a good sensor-skin interface:

Next to placing the sensor in the middle of the belly of the muscle, an effective electrode-skin contact will provide great benefits in assuring a high quality signal.

Method of application:

- 1. Shave excessive hairs, although in most cases the hair can simply be moved aside or sensor can be placed over hair.
- 2. Clean skin with alcohol to remove skin debris. Allow alcohol to evaporate. (When using Delsys sensors, abrasion of the skin is NOT required.)
- 3. In most cases (depending on skin type) no electrolyte is required.
- 4. Attach sensor-skin interface. Press hard to assure maximal adhesion to the skin.

The quality of the adhesive capability of the sensor and its response to mechanical perturbations have been tested as shown in the following slides.

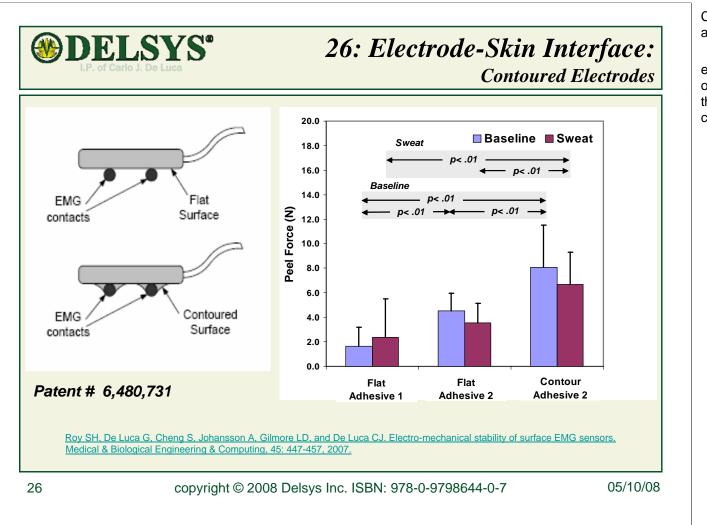


Tests of sensor adhesion to skin:

In the referenced study, we developed tests and procedures for designing the contact surface of sEMG sensors. Specifically we evaluated different sensor designs and different interfaces between the sensor and the skin to determine how they affected sensor performance under conditions of sweat accumulation on the skin (sweat test) and when mechanically disturbed by impact and sinusoidal forces.

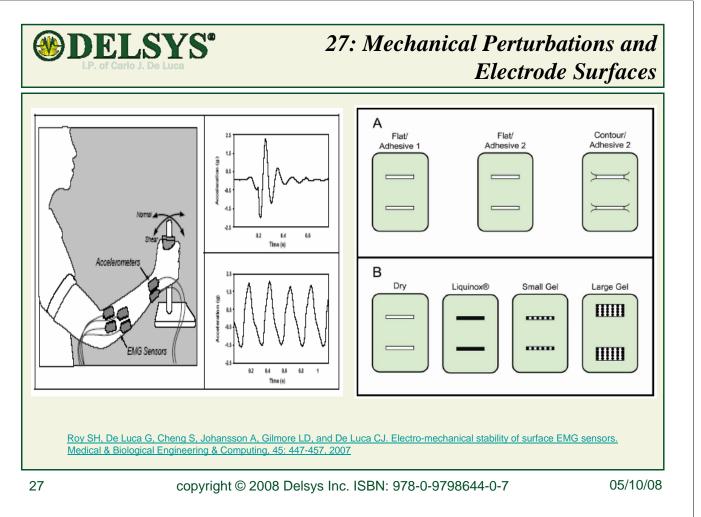
In one series of tests we evaluated how well the sensor remains affixed to the skin when differently shaped sensors were peeled by a mechanical device (shown above). We were specifically interested in evaluating whether contouring the skin surface of electrode improves performance.

In another series of test we evaluated the effect that conductive gels and other preparations have on reducing artifact when the sensors are perturbed.



Contoured electrodes improve ability of adhesive to attach:

The contoured edges around the electrodes significantly increased the amount of force required to peel the sensor away from the skin, implying that it enables a better contact between the sensor and the skin.

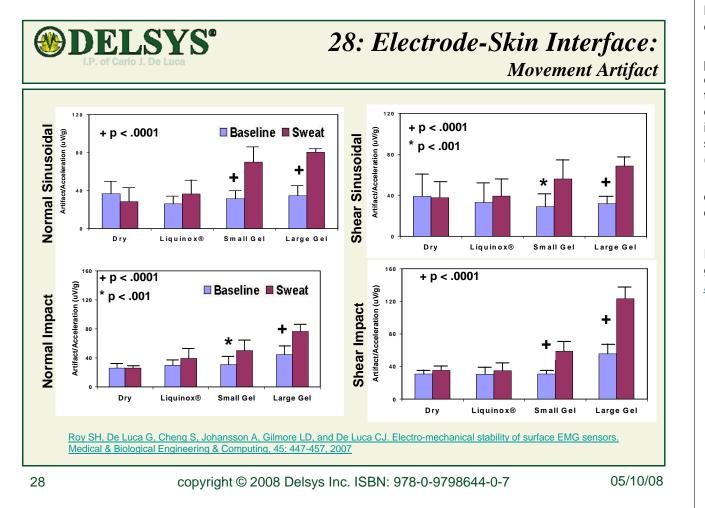


Mechanical perturbations and electrode surfaces:

This was a test for establishing the influence of various electrolytes between the electrode and the skin on the generation of a movement artifact. (These are commonly used to improve the electrical conductivity between the electrode and the skin.) We also tested the performance of the sensor with no applied electrolyte.

Mechanical disturbances were applied as a sinusoidal force in the normal and shear direction, and also as an impact in the normal and shear direction.

The disturbance on the skin was monitored with accelerometers and the artifact was monitored by the sensors. See next slide for results.

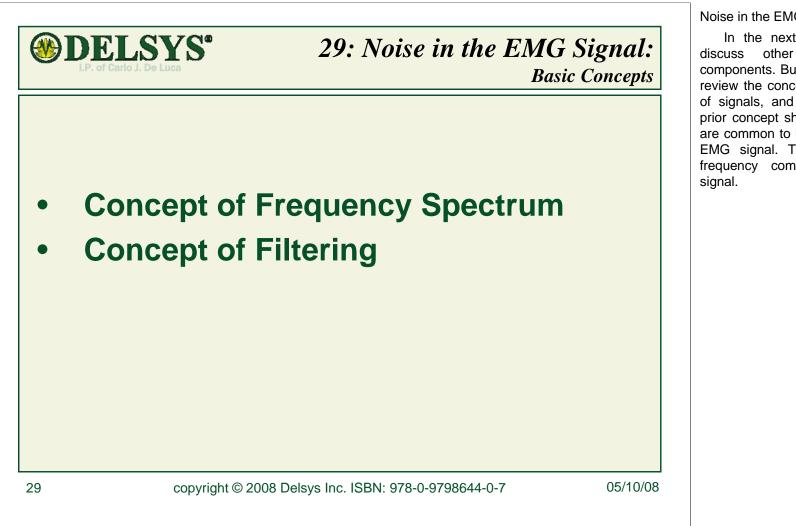


Movement artifact and the influence of electrolyte contact:

The results of the mechanical perturbations demonstrated that the gel electrolyte performed poorly and worsened in the presence of sweat. The dry electrode (no electrolyte) generally performed the best in the impact test, and the performance was statistically similar to that of the second best (Liquinox) in the shear sinusoidal test.

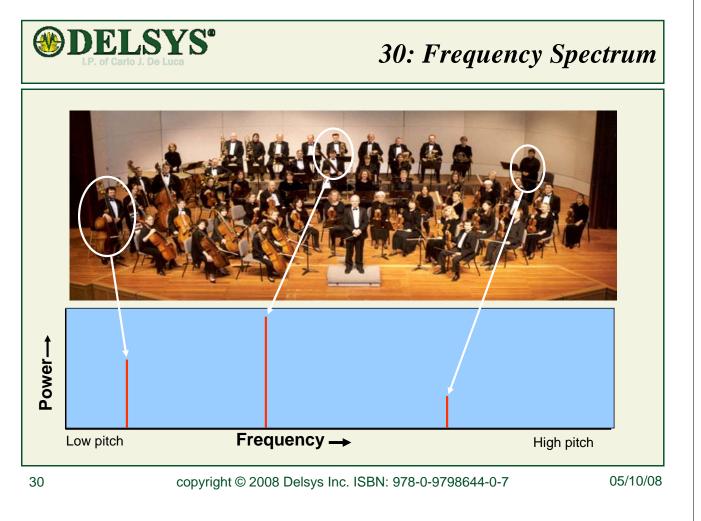
Note that the impact test represents the disturbance profile on the lower limb that occurs during walking.

FOR MORE INFORMATION ON SENSORS go to the end of the presentation to <u>Appendix</u> <u>A: sEMG Sensor Factors.</u>



Noise in the EMG signal:

In the next sequence of slides we will discuss other characteristics of noise components. But in order to do so we need to review the concept of the frequency spectrum of signals, and the concept of filtering. The prior concept shows the frequency range that are common to both the noise signals and the EMG signal. The latter removes unwanted frequency components from the detected

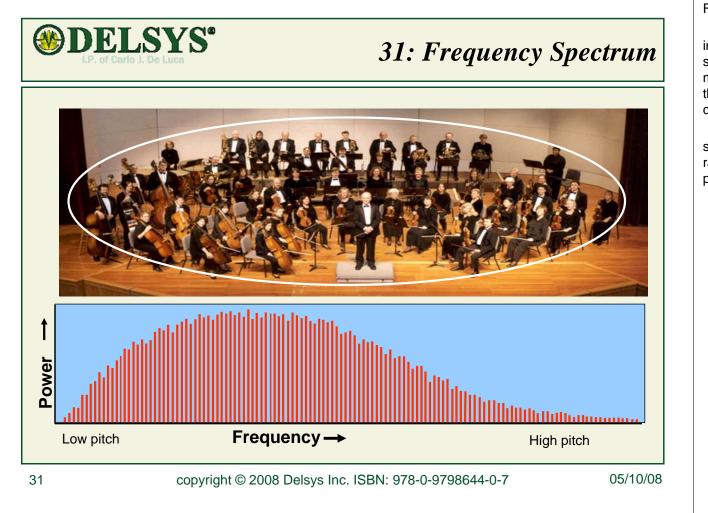


Frequency spectrum:

The concept of a frequency spectrum can be difficult to grasp for a novice. The frequency spectrum of the EMG signal can be understood by drawing a parallel to the sound emanating from an orchestra. Consider the arrangement of the instruments in an orchestra. (To simplify the comparison the arrangement of instruments in the above figure has been inverted with the base section on the left and the violin section on the right.)

When a single base plays a note it emits a relatively low frequency (pitch) sound. A single frequency contribution to the spectrum is made in the spectrum plot below at the corresponding frequency value. The height of the contribution (the bar) corresponds to the loudness (amplitude) of the note.

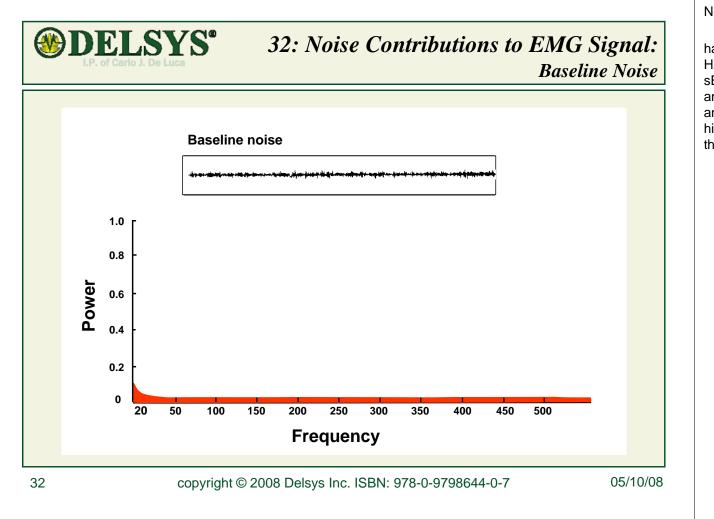
A similar operation is performed for a violin having higher pitch (frequency) and for an instrument located in the middle of the orchestra, having an intermediate frequency.



Frequency spectrum:

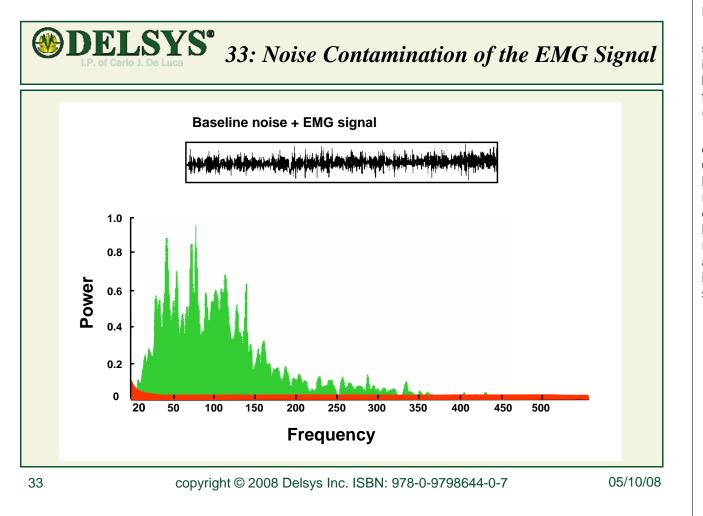
When all the instruments play, the individual frequency contributions fill the spectrum. And as the orchestra, in unison, modulates the amplitude of all the instruments the envelope of the spectrum modulates correspondingly.

The frequency spectrum of the sEMG signal is constructed in a similar fashion, with a range from 0 to approximately 450 Hz, with a peak in the neighborhood of 80 to 100 Hz.



Noise contributions to the EMG signal:

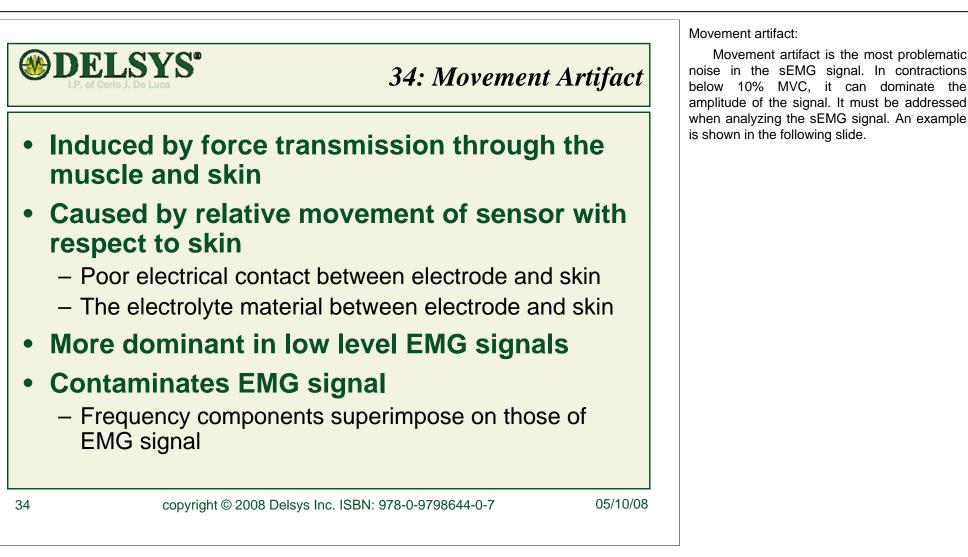
The baseline noise of the recording system has a frequency spectrum that ranges from 0 Hz to a frequency range much greater than the sEMG signal (several thousand Hz). The amplitude is greater at the low frequency end and tapers to a near constant amplitude at higher frequencies, still within the bandwidth of the sEMG signal frequency spectrum.

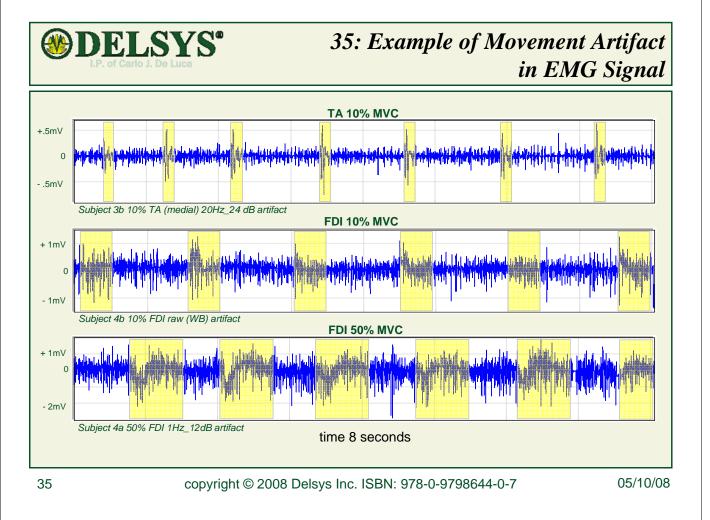


Noise contributions to the EMG signal:

The signal in the box consists of the sEMG signal and the baseline noise. Note that there is no visible indication of the presence of baseline noise. The corresponding spectra of the baseline noise (red) and the sEMG signal (green) can be seen in the plot.

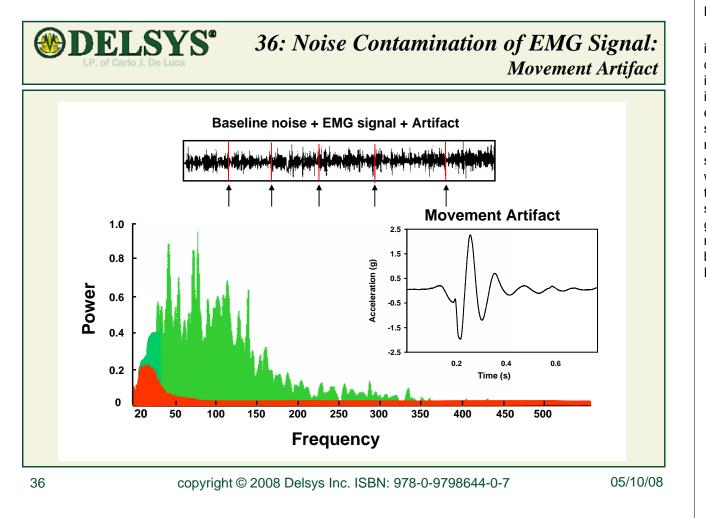
The noise spectrum has the characteristics of 1/f noise, which has its highest amplitude at 0 Hz. It quickly decreases to a near constant level by 10 to 20 Hz. This is an example of the relative amplitudes measured during a weak contraction (say 10% MVC). During higher level contractions, the baseline noise signal remains constant and the sEMG signal amplitude increases. Hence, the baseline noise is obviously a greater concern for sEMG signals acquired during weak contractions.





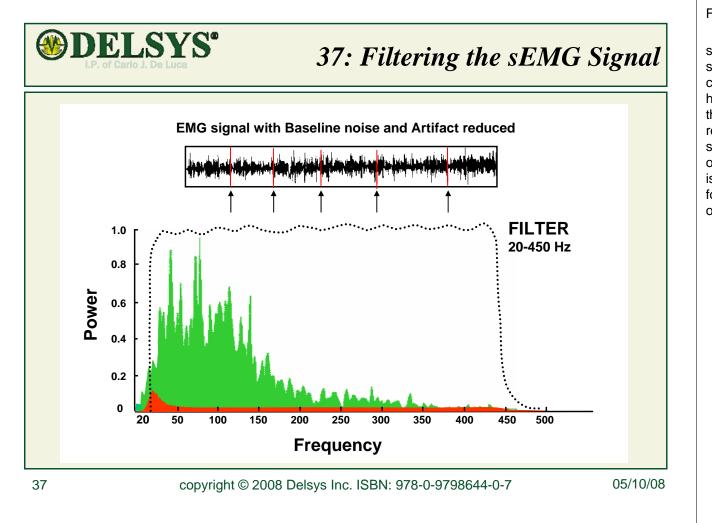
Example of movement artifact in EMG signal:

The movement artifacts are highlighted in yellow in these sample EMG signals. Notice that at low contraction levels, the movement artifact can significantly alter the amplitude of the signal and may cause confusion in the interpretation of the sEMG signal, as the artifact appears to be part of the sEMG signal. At higher contraction levels, the movement artifact may be harder to identify within the EMG signal.



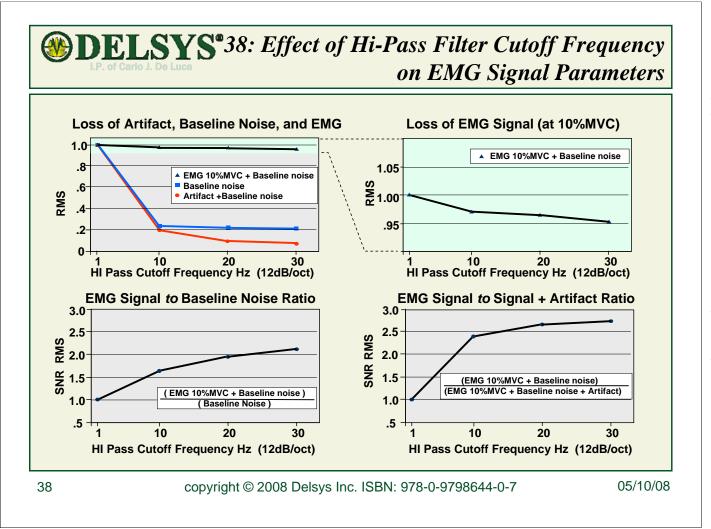
Noise contributions to the EMG signal:

The signal in the box at the top of the slide is an sEMG signal acquired during a contraction in which a movement artifact was induced. The location of the movement artifact is indicated by the vertical arrows. An expanded plot of the movement artifact is shown in the lower frame on the right. This motion artifact is comparable in amplitude and shape to that caused during a heel strike while walking. The frequency spectrum of this artifact together with that of the baseline noise is shown in red. Note that it has a considerably greater amplitude than that of the baseline noise (shown in a previous slide) and the bandwidth generally ranges from 0 Hz to 50 Hz, occasionally it may be higher.



Filtering the EMG signal:

The spectra of both noise sources are shown superimposed on that of the sEMG signal. Much, but not all of their contribution can be removed by judicious filtering. At the high end, a cut-off point at 450 Hz truncates the contribution from the baseline noise without removing any significant contribution from the sEMG signal. At the low-frequency end, a cutoff point at 20 Hz is recommended. This point is contested by other investigators, but the following slide will present evidence in support of this position.



Effect of Hi-Pass filter cutoff frequency on EMG signal parameters:

Top left panel -- Losses in the RMS value of the sEMG signal (black), the Baseline noise (blue), and the movement artifact (red) when the signal is filtered with a high-pass (lowfrequency cut-off) at 1, 10, 20 and 30 Hz. Approximately 80% of the noise is removed at 10 Hz, with only 3% loss in the sEMG signal (top right panel). However, an additional 10% of the movement artifact is removed at 20 Hz, with no appreciable additional loss of sEMG signal. Filtering at 30 Hz does not appear to provide any real benefits in noise reduction, while it removes approximately an additional 1% of the sEMG signal.

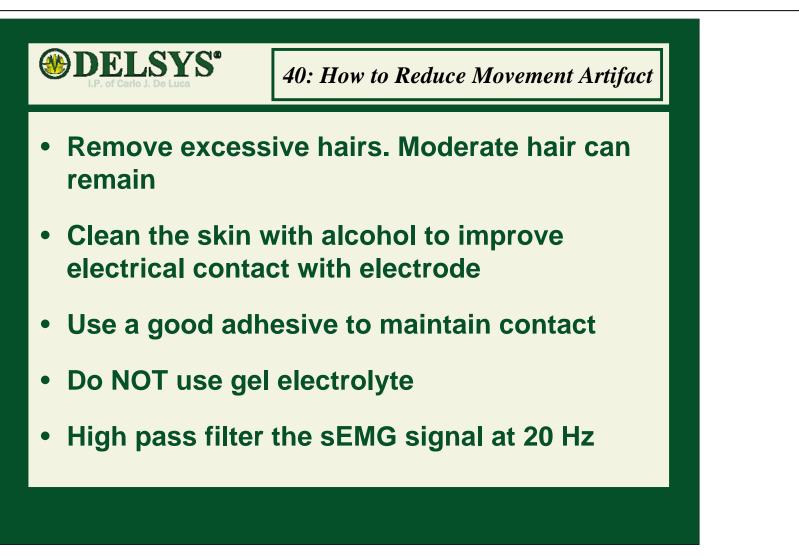
The benefit of filtering at 20 Hz may be seen in the bottom two panes, where the signal to noise ratio increases only marginally at 30 Hz. It should be noted that for movement artifacts having a wider bandwidth, the cut-off frequency should be greater than 20 Hz.

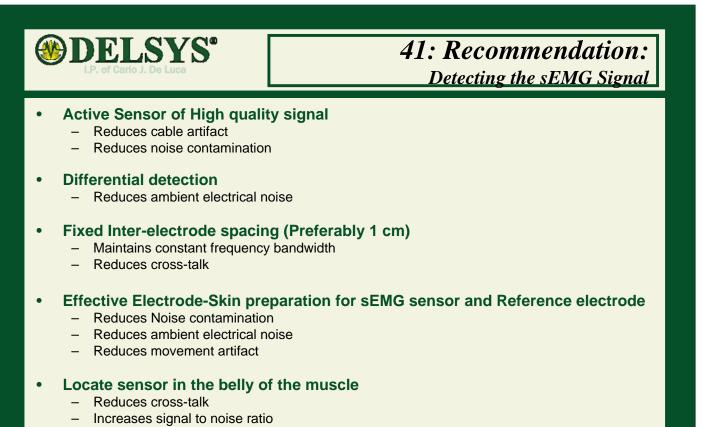
39: Effect of Hi-Pass Filtering Compared to Sensor Location		
High Pass -3dB 10Hz → 20Hz	Slope dB/oct 12dB → 24dB	<u>Shift</u> 2cm
<b>↓</b> 10 - 50%	<b>↓</b> <13%	
<ul> <li>✓ &lt;2%</li> <li>✓ &lt;4%</li> </ul>	<b>↓</b> <1% <b>↓</b> <3%	19 - 38% 19 - 38%
<b>↑</b> <3%	<b>↑</b> <1%	10 - 20%
<b>1</b> 20 - 36%	<b>1</b> 4 -10%	
<b>†</b> 11 - 28%	<b>¢</b> <7%	
	Example 10 - 20 - 36%	Compared to SensHigh Pass -3dBSlope dB/oct $10Hz \rightarrow 20Hz$ $12dB \rightarrow 24dB$ $10Hz \rightarrow 20Hz$ $12dB \rightarrow 24dB$ $10 - 20\%$ $4<6\%$ $4 - 10\%$ $4<6\%$ $4 - 2\%$ $4<1\%$ $4 - 3\%$ $4<-1\%$ $4 - 3\%$ $4 - 10\%$

Effect of hi-pass filtering compared to sensor ocation:

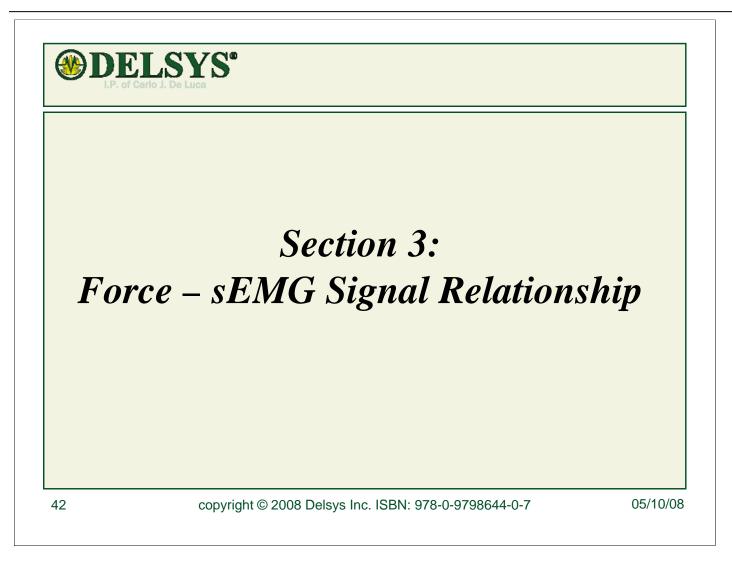
Note that a 1 cm shift in the location of the sensor introduces a dramatic variation in the amplitude of the sEMG signal, in the range of 10 to 40%. This is far greater than that resulting from filtering. Thus, in terms of amplitude consistency, electrode positioning (inter-subject comparison) and re-positioning (intra-subject comparison) is more important for obtaining a greater signal to noise ratio.

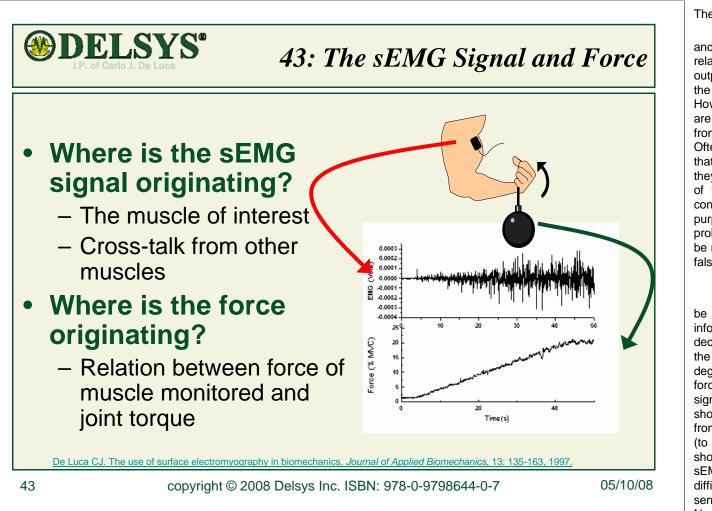
FOR MORE INFORMATION ON SENSORS go to Appendix A: sEMG Sensor Factors.





- Do not place sensor on the tendon or on the innervation zone

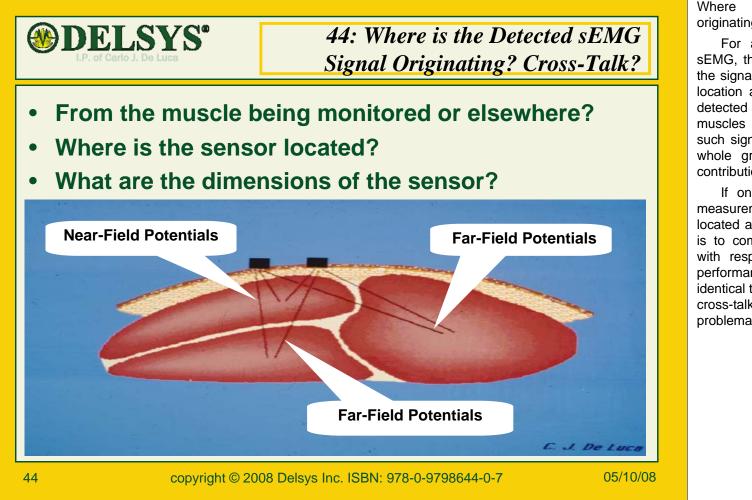




## The SEMG signal and the Force:

The panel on the right illustrates the most basic and most used property of the sEMG signal, the relationship between the sEMG signal and the force output of a muscle. Note that as the amplitude of the sEMG signal increases, so does the force. However, the detected force and the sEMG signal are almost always contaminated by contributions from other muscles (this is referred to as cross-talk). Often, investigators use technology and techniques that yield higher amplitude signals believing that they have higher fidelity signals, whereas the quality of the detected signal is likely compromised by contributions from other muscles. For some purposes this contamination may not be problematic, but for finer, more precise work it can be misleading, causing improper interpretations and false conclusions.

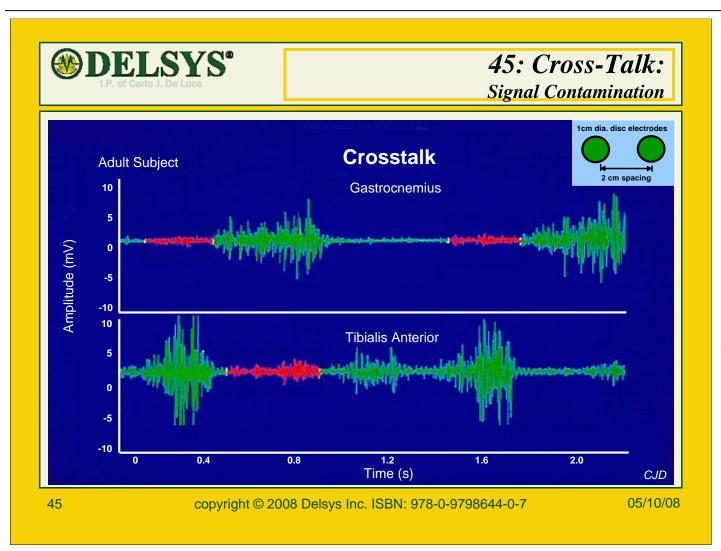
The detected sEMG signal and force that are to be analyzed for physiological or biomechanical information will provide incorrect, and perhaps even deceptive information if the two questions posed in the slide cannot be answered with a reasonable degree of assurance. If one intends to relate the force produced by a specific muscle with the sEMG signal detected by a sensor, then the sEMG sensor should be minimally contaminated with information from other muscles (cross-talk) and noise sources (to be discussed later) and the recorded force should originate from the muscle on which the sEMG sensor is placed. The latter point may be difficult to achieve as externally located force sensors measure the torque at a ioint. Nonetheless, all efforts should be made to maintain linearity between the change in the force and the change in the sEMG signal so that the relative comparison remains correct.



Where is the detected sEMG signal originating? Cross-talk?

For accurate and proper application of sEMG, the user should consider the origin of the signal. If a sensor is placed in a particular location above a group of muscles, then the detected sEMG signal will originate from all the muscles in the proximity. The information in such signals is limited to the activation of the whole group of muscles and to the force contribution of the group of muscles.

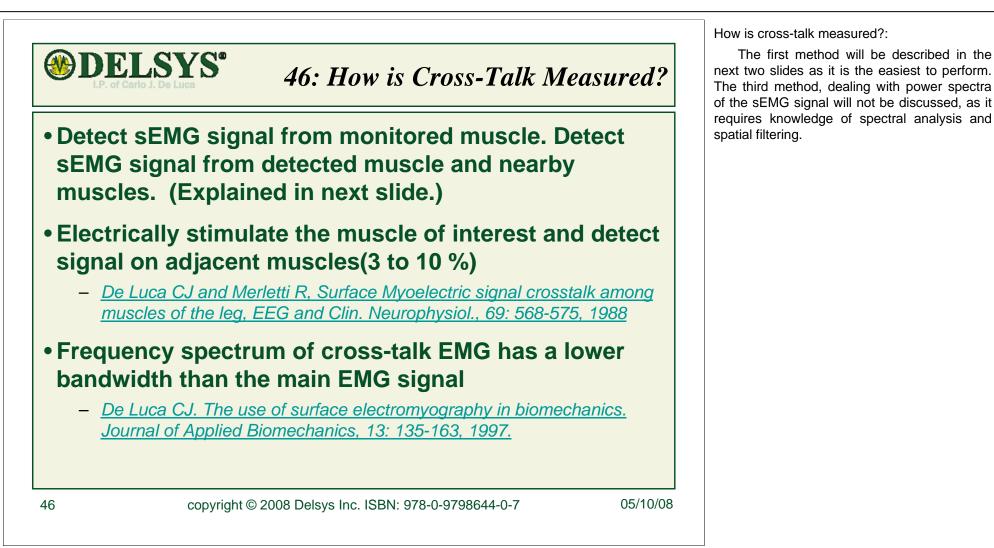
If one wishes to perform more precise measurements, then the sensor should be located above individual muscles. If the intent is to compare the performance of a muscle with respect to another or to compare the performance of one muscle performing identical tasks among several subjects than the cross-talk from adjacent muscles becomes problematic.

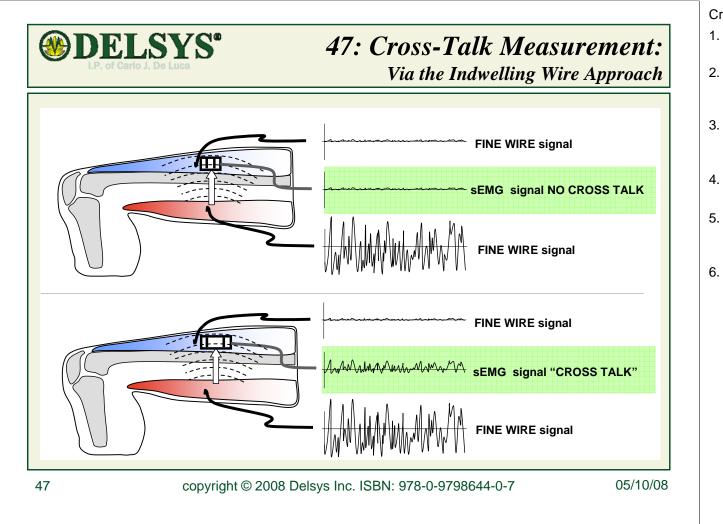


## Cross-talk: Signal Contamination:

The use of sensors with large electrode area and large inter-electrode spacing invariably leads to detection of cross-talk which is often misinterpreted as activity from the monitored muscle. In clinical applications this misunderstanding may lead to false diagnosis. In the research field it may lead to a basic misunderstanding of the performance of the monitored muscle.

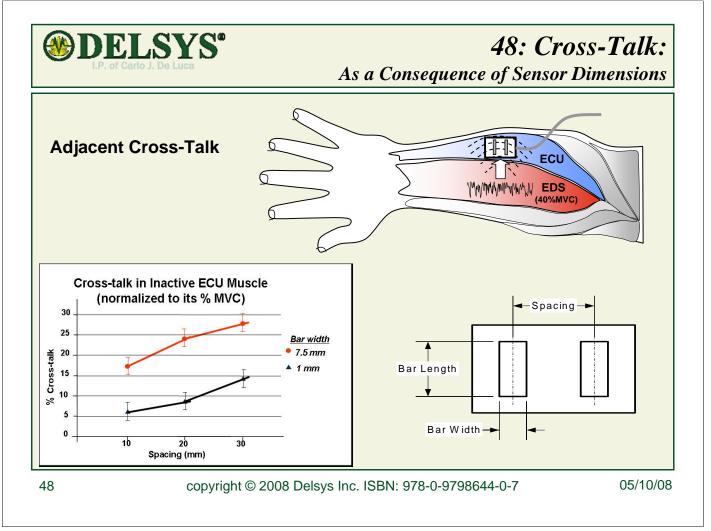
The data for this example were collected during a gait cycle of a normal subject with the sensor configuration shown in the top right hand corner. Note that the signal highlighted in red is a cross-talk signal that originates in the other monitored muscle. With sensors having smaller electrodes and shorter inter-electrode spacing, the cross-talk signal would be substantially smaller. Proof will be provided in the following slides.





Cross-Talk measurement:

- 1. Place a fine-wire sensor in the muscle (red) generating a cross-talk signal.
- 2. Place an sEMG sensor and a fine-wire sensor on and in the muscle (blue) to be monitored.
- Relax the muscle that is monitored (blue) verify by lack of activity in both the surface and indwelling sensors. -- <u>Top Panel</u>
- 4. Contract the muscle (red) that generates cross-talk.
- If there is no signal from the fine wire and surface sensors, then there is NO crosstalk -- <u>Top Panel</u>
- 6. If there is no signal from the fine wire sensor and there is a signal from the surface sensor, then there **IS** cross-talk. --<u>Bottom Panel</u>

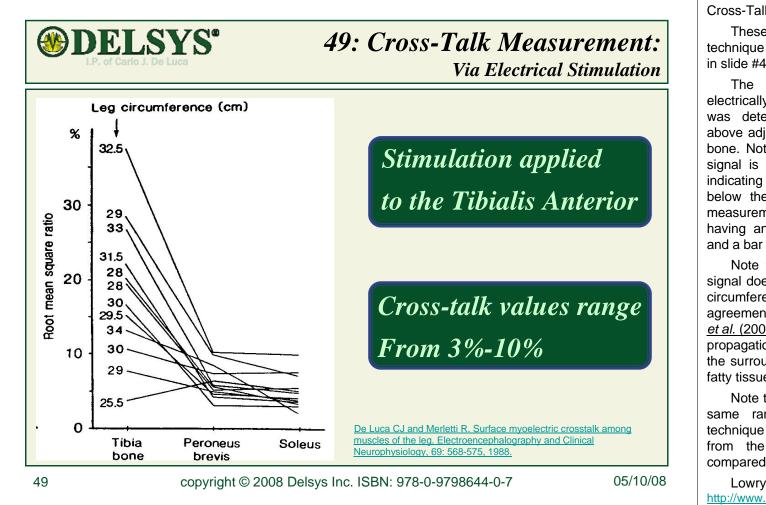


## Cross-Talk and Sensor Dimensions:

The amount of cross-talk detected is greatly affected by the dimensions of the sEMG sensor. Cross-talk measurements were made on the Extensor Carpi Ulnaris with surface sensors whose electrode surface and inter-electrode spacing varied.

Note that as the inter-electrode spacing and the area of the electrode increase, the cross-talk increases. The 1 cm inter-electrode spacing and the 1 mm thick electrode has the lowest cross-talk of all the tested combinations. Note that the commonly used sensor dimensions of 2 cm inter-electrode spacing and the electrode dimensions of 7.5 X 10 mm detects 4 times the amount of cross-talk as the 1mm X 10mm.

It follows that smaller than 1 cm interelectrode spacing might produce even less cross-talk. However, practical issues such as electrical shorting of the electrodes during sweating and lower signal amplitudes become a concern.



Cross-Talk from Electrical Stimulation:

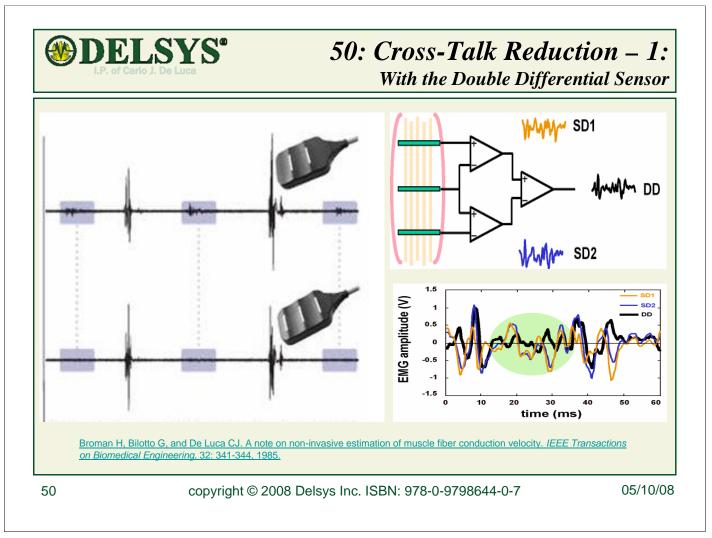
These are results from the second technique for measuring cross-talk described in slide #47.

The Tibialis Anterior muscle was electrically stimulated and the sEMG signal was detected above the Tibialis Anterior, above adjacent muscles, and above the Tibial bone. Note that in this arrangement an EMG signal is detected on top of a bone, clearly indicating that the signal does not originate below the sensor. The sensor used in this measurement was a Delsys DE2.1 sensor having an inter-electrode spacing of 10 mm and a bar width of 1 mm.

Note that the amplitude of the cross-talk signal does not appear to be correlated to the circumference of the leg, a point that is in agreement with the modeling work of Lowry M. <u>et al. (2007)</u> which showed that the EMG signal propagation is influenced by the anisotropy of the surrounding tissue, specifically the ratio of fatty tissue to muscle tissue.

Note that the amount of cross-talk is in the same range as that measured with the technique in the previous slide, if the cross-talk from the 1mm X 10mm bar sensor is compared.

Lowry et al. 2007 on pubmed: http://www.ncbi.nlm.nih.gov/sites/entrez?db=pubme d&uid=17482677&cmd=showdetailview&indexed=g oogle

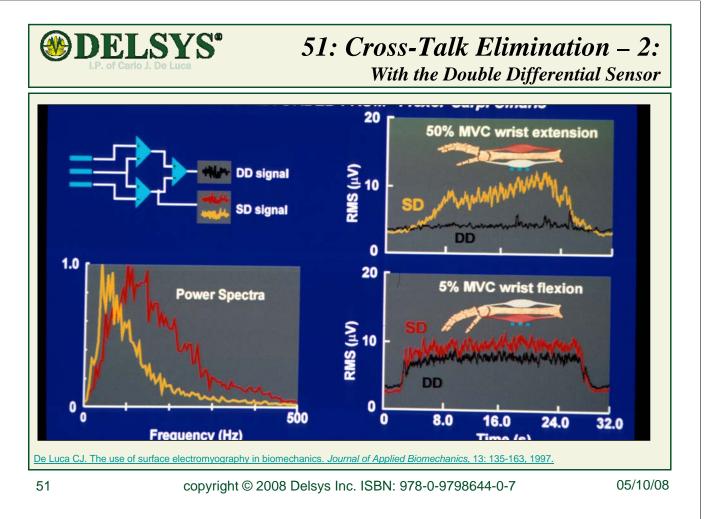


Cross-talk elimination with the double differential sensor:

The simplest practical method for reducing cross-talk is to use the double differential (DD) sensor, first described in the above reference. As may be seen in the top right-hand quadrant, the DD sensor consists of two stages of differential amplification. A non-common mode signal such as a cross-talk signal originating from adjacent muscles, will not be removed by the signal differential (SD) amplification. However, at the input of DD amplification, the cross-talk signal appears as a common-mode signal and is, in large part, eliminated by the DD amplification. This point is illuminated in the panel at the bottom right which presents the signals at the output of the SD amplification stage and the signal at the output of the DD stage. The green shaded region shows the DD signal (black) having lower amplitude that the SD signals (orange and blue). In the time interval highlighted by the green region, the amplitude of the DD signal is lower than both the SD signals, indicating that some cross-talk signal has been eliminated.

The performance of the DD sensor may be seen in the panel on the left where the sEMG signal was detected simultaneously from the Flexor Carpi Radialis muscle with a SD sensor and a DD sensor. The shaded areas indicate a crosstalk signal that is eliminated in the signal detected by the DD sensor.

FOR MORE INFORMATION ON SENSORS go to <u>Appendix A: sEMG Sensor</u> <u>Factors.</u>



This slide shows how the Double Differential (DD) sensor reduces cross-talk or can be used to reduce the presence of cross-talk (black signal).

Another example showing the effectiveness of the Double Differential (DD) sensor for eliminating cross-talk:

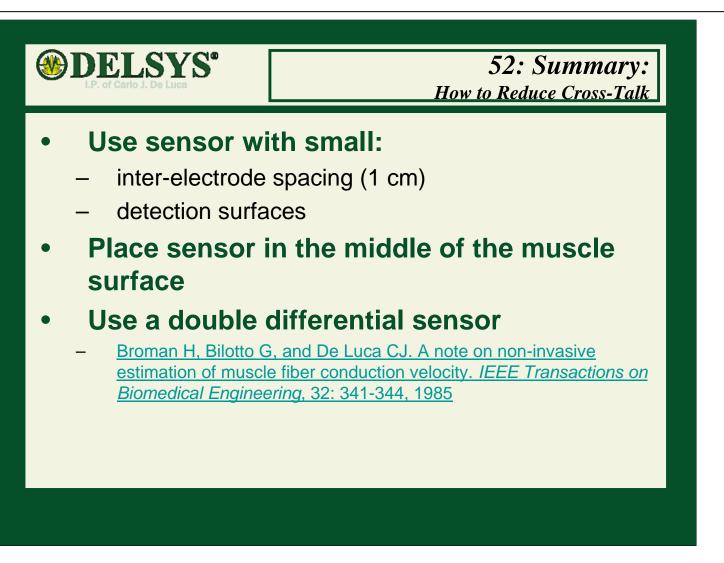
The <u>top left panel</u> shows the DD configuration along with a tap on a single differential (SD) configuration. (Note that the SD configuration tap is not available from the commercial version of the DD sensor.) This sensor detects both the SD sEMG signal and the DD sEMG signal.

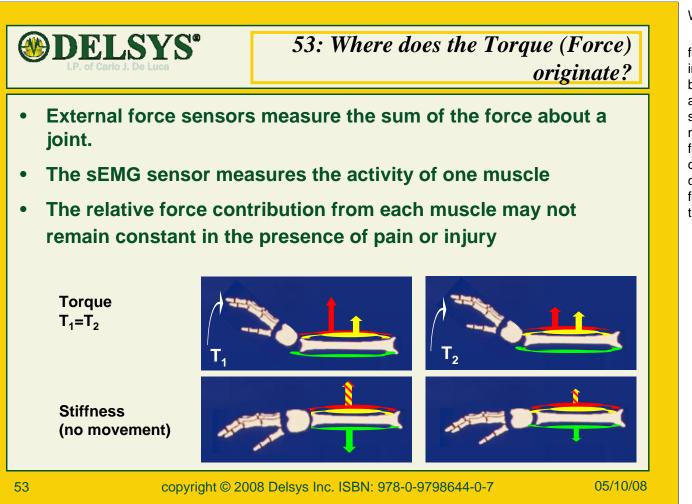
In the two panels on the right, the sensor is placed on Flexor Carpi Ulnaris. In the top right panel a strong 50% MVC extension contraction is performed; in the bottom right panel a weak 5% MVC flexion contraction is performed.

The <u>top right panel</u> shows during a strong contraction, only a weak (<10 uV) SD sEMG signal (yellow) is detected and virtually no DD sEMG signal (black). Because the signal is weak, it does not originate from the muscle below the sensor, and must originate from the contracting antagonist muscle (Extensor Carpi Ulnaris). Thus it is a crosstalk signal and it is eliminated by the DD detection (black).

The <u>bottom right panel</u> shows that during a weak flexion contraction, a weak SD sEMG signal (red) and a similarly weak DD sEMG signal are detected indicating the signals detected by both configurations originates in the nearby flexor muscle. If the signal had originated elsewhere the SD signal would be small (as seen in the previous panel) and the DD signal would be near zero.

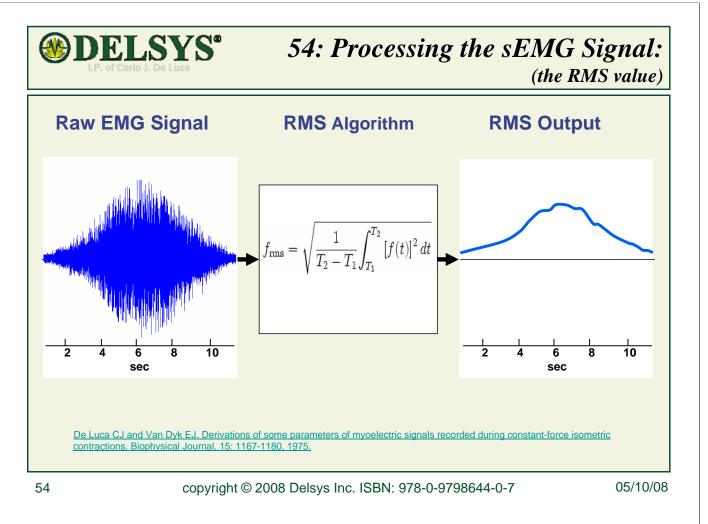
The bottom left panel shows the frequency spectra of the SD sEMG signals during weak flexion (red) and strong extension (yellow). Note that in the spectrum of the SD sEMG signal from the extension contraction (yellow) the higher frequencies are considerably attenuated. This is indicative of "spatial filtering" which acts as a low-pass filter (one that removes higher frequencies) when the signal must travel through the tissues of the body. This observation supports the notion that the SD signal originates at a greater distance, or from some other muscle.





Where does the torque (force) originate?:

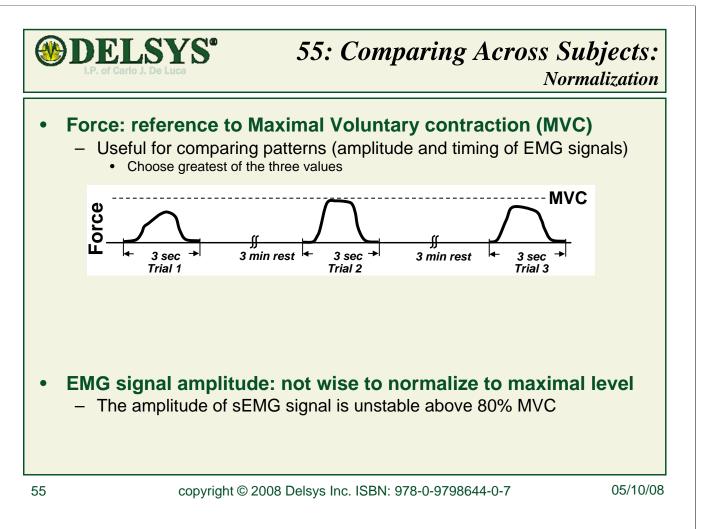
When the sEMG signal is related to the force being generated by the muscle, it is important to understand the relationship between the measured force and the force actually being produced by the muscle. As is seen in the diagram, the force or torque measured about a joint is the sum of all the forces acting on that joint. When more than one muscle is active, there are many finite combinations of synergist and antagonist forces that can produce a given torque about the joint.



Processing the sEMG signal (the RMS value):

The raw EMG signal must be processed before it can be used for most scientific purposes. The Root-Mean-Squared (RMS) value provides a measure of a physical property of the EMG signal, that is the energy of the signal. This makes it a more useful way of conceptualizing the EMG signal than other mathematical functions which have been used in the past, such as the mean rectified value and the integrated value.

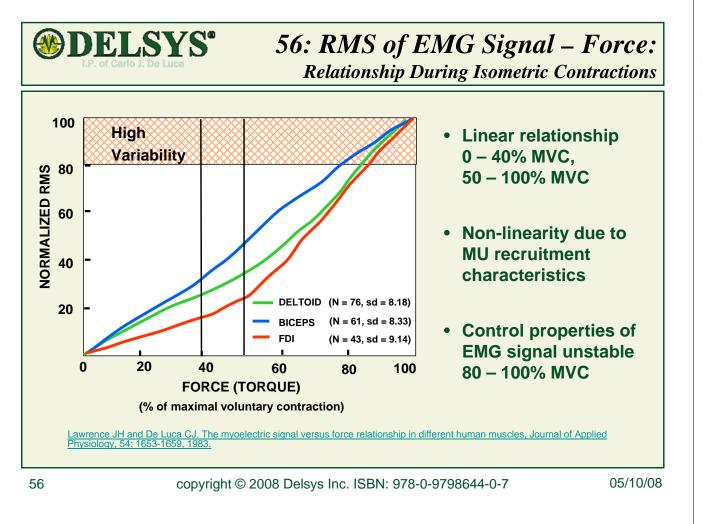
Let the sEMG signal be represented by f(t). It is known that the amplitude of f(t) is a random value and can be approximated by a Gaussian distribution function (numerous references in the literature). The RMS function processes the signal to render a filtered and thus smooth amplitude. The greater the time interval T2 – T1, the greater the amount of filtering or smoothing.



Comparing across subjects or comparing among different trials performed at different times (normalization):

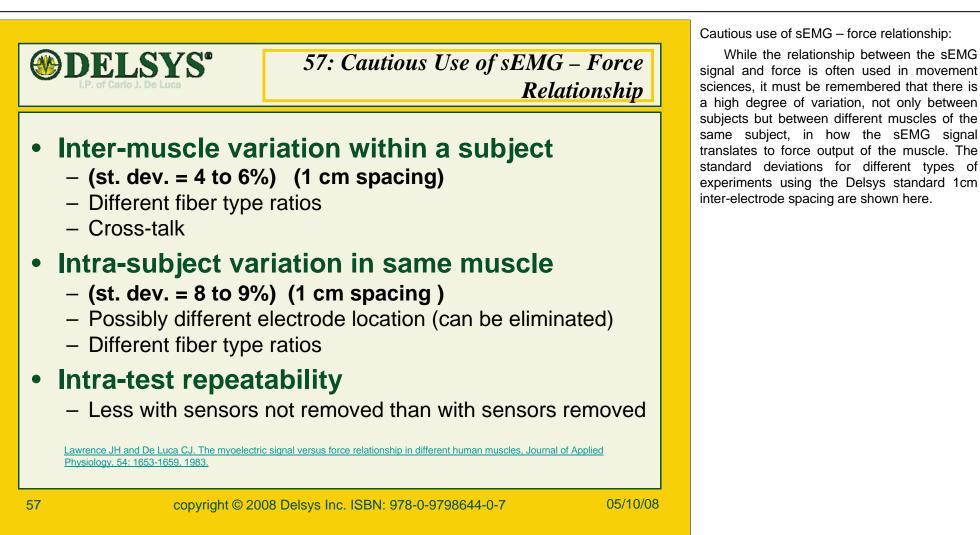
In several of the previous slides it has been indicated that the amplitude of the sEMG signal may be influenced by a variety of factors unrelated to the physiological properties of the muscle. Yet sometimes it can be useful to compare the sEMG signal obtained from the same muscle in multiple subjects performing similar tasks, or to compare the sEMG signal from the same muscle of the same subject, but performed during different tests, say on different days. While the absolute value of the sEMG signal varies widely across subjects, we can normalize the signals to some constant value. The point of reference chosen depends on the data of interest. Often, the maximal voluntary contraction (MVC), or strongest contraction the subject can perform with that muscle when asked, is used as a reference point.

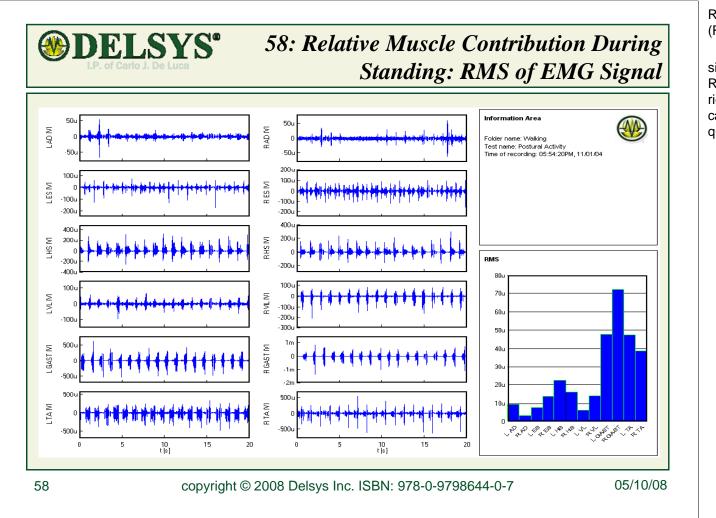
Note that even if the contraction is performed at the same force level, as would be the case for holding a weight, the sEMG signal must still be normalized if the sensors are removed between trials, especially if the trials are performed at different times.



RMS of sEMG signal – force relationship during isometric contractions:

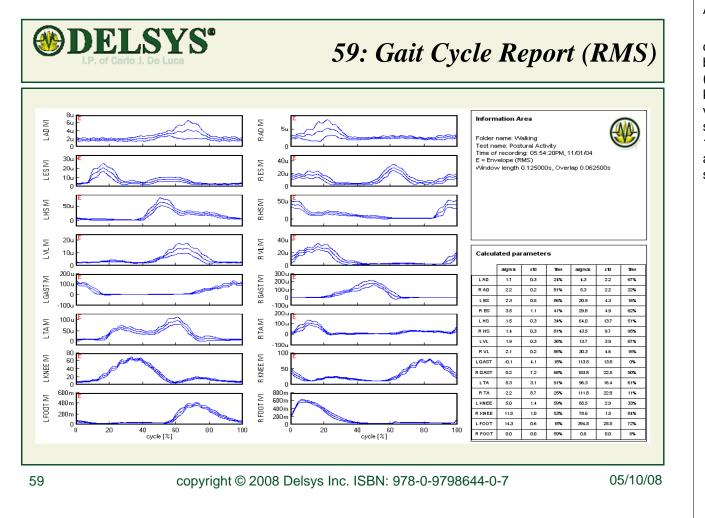
At contraction levels above 80% MVC the firings of the high threshold motor units are unstable. Motor unit action potentials from high threshold motor units have relatively higher amplitude, they fire slower, and they are recruited and derecruited as the force level fluctuates. In contrast, low threshold motor units have lower amplitude action potentials, and a greater frequency of firing.





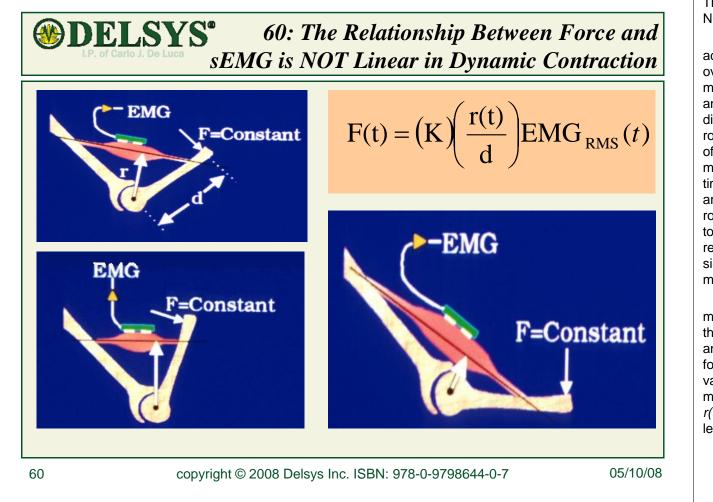
Relative muscle contribution during standing (RMS of EMG signal):

See here an example of the raw EMG signal (in left quadrants) and the corresponding RMS values of the individual muscles (bottom right quadrant). In this case, the RMS value is calculated over the epoch presented in the quadrants.



An example of Intra-test variability:

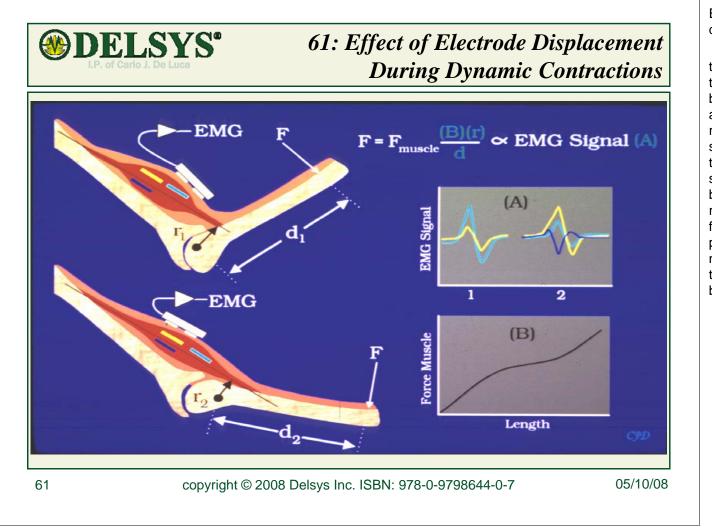
The mean (center trace) and the standard deviation (upper and lower trace) of the cyclic behavior of muscles in the back and lower limb (first six panels) and the joint angles of the knee and ankle during a gait step. These values were calculated by averaging over 12 steps whose time duration was normalized to 100%. In each step, the initiation of EMG activity had to be identified in order to synchronize the epochs.



The relationship between force and sEMG is NOT linear in dynamic contraction:

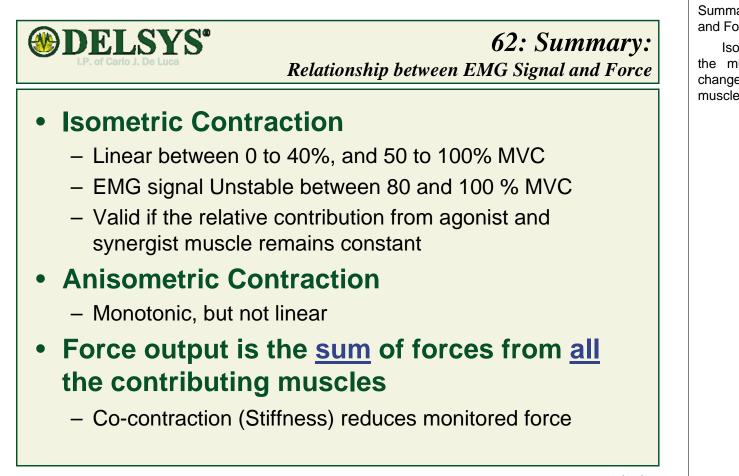
Consider the case of a single muscle acting on a joint. When the muscle contracts over a period of time - t -, the length of the muscle shortens, the joint angle decreases, and the moment arm of the muscle (the distance from the muscle to the center of rotation of the joint) increases. The time course of this distance is defined as r(t). The monitored torgue is equal to the force - F times the distance - d -, where d is the moment arm of the measured force to the center of rotation. Thus we can write the equation in the top right quadrant where K is the factor that relates the RMS value of the monitored sEMG signal to the force produced by the contracting muscle.

Now consider the case where the monitored force - F - remains constant during the shortening contraction. From the equation and from the pictorial of the other quadrants it follows that the relationship between The RMS value of the monitored sEMG signal and the monitored force changes. As the moment arm r(t) decreases the force produced by the lengthening muscle must increase.



Effect of electrode Displacement during dynamic contractions:

During a dynamic contraction, in addition to the change in the moment arm, there are two other factors that add to the nonlinearity between the force output and the EMG signal amplitude. The first factor is the change in the relative position of the source of the EMG signal and the sensor which remains attached to the skin as the muscle moves below the skin. This factor changes the spatial filter between the signal origin and the sensor, rendering a change in the amplitude and frequency spectrum of the signal. (See top panel on the right.) The second factor is the non-linear relationship of the force produced by the muscle and the length of the muscle. (See bottom panel on the right.)

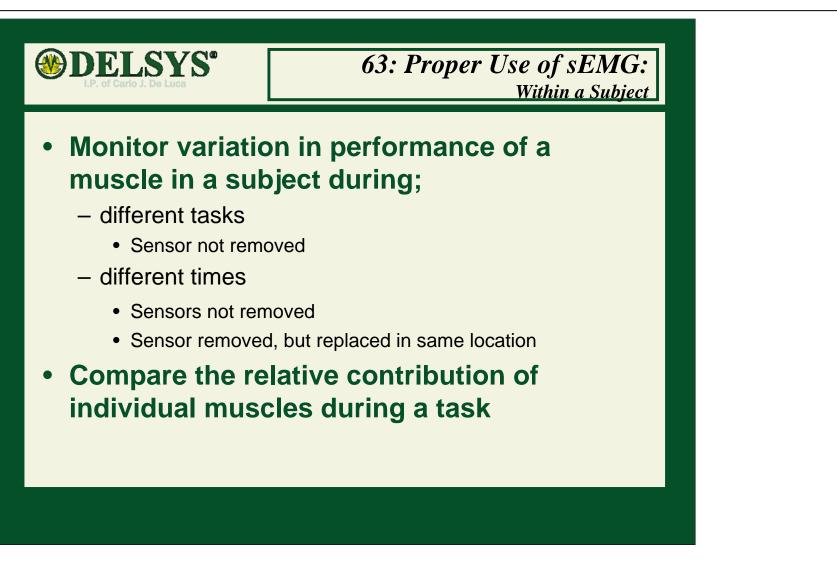


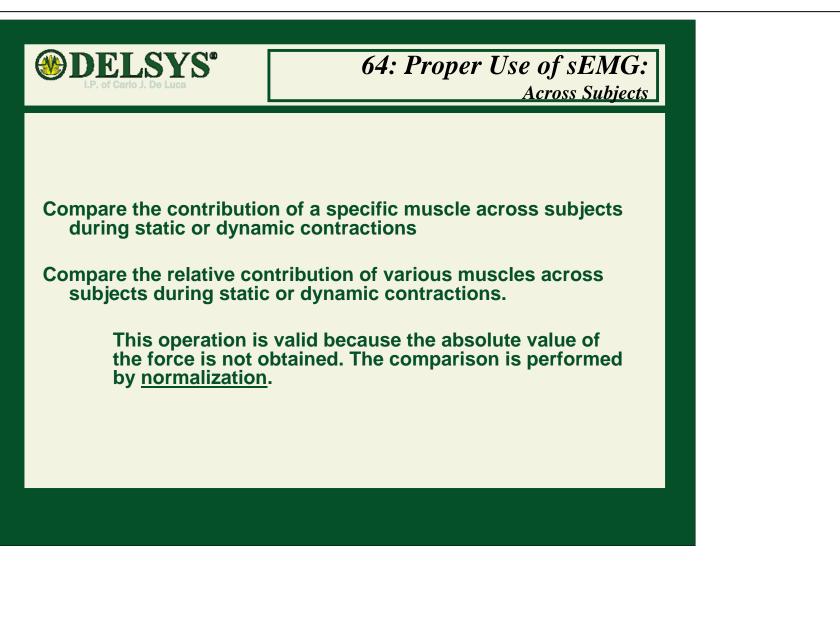
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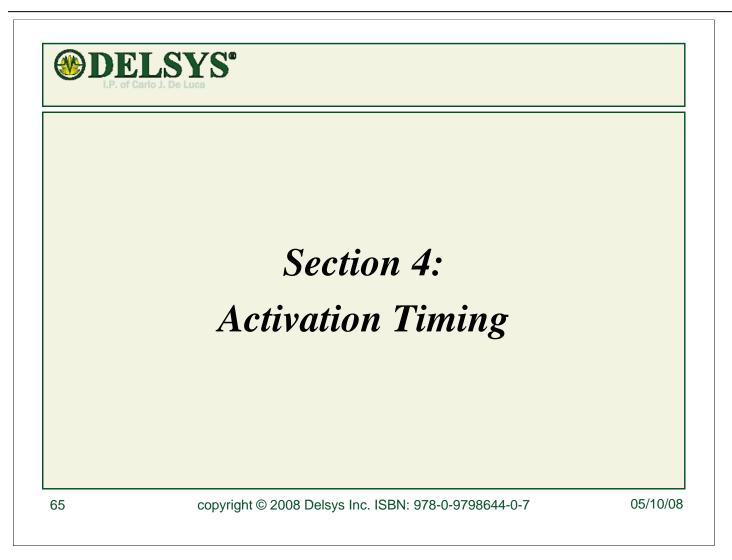
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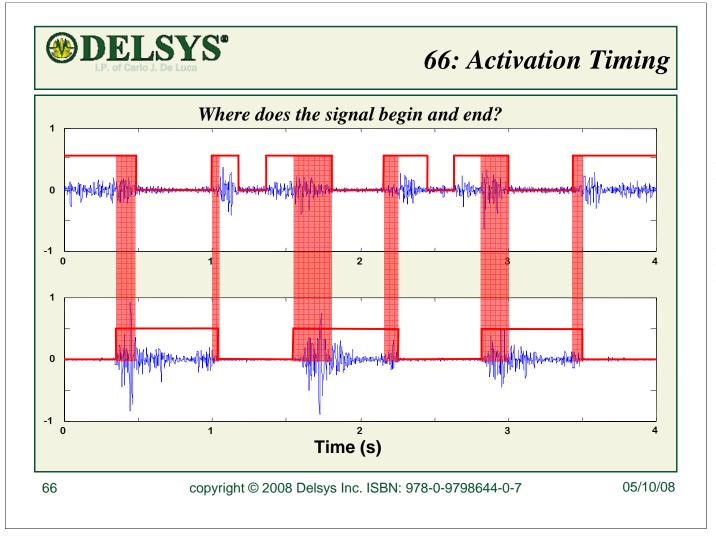
Summary – Relationship between EMG signal and Force:

Isometric contractions are those in which the muscle produces force, but does not change length. In anisometric contractions, the muscle is allowed to lengthen or contract.





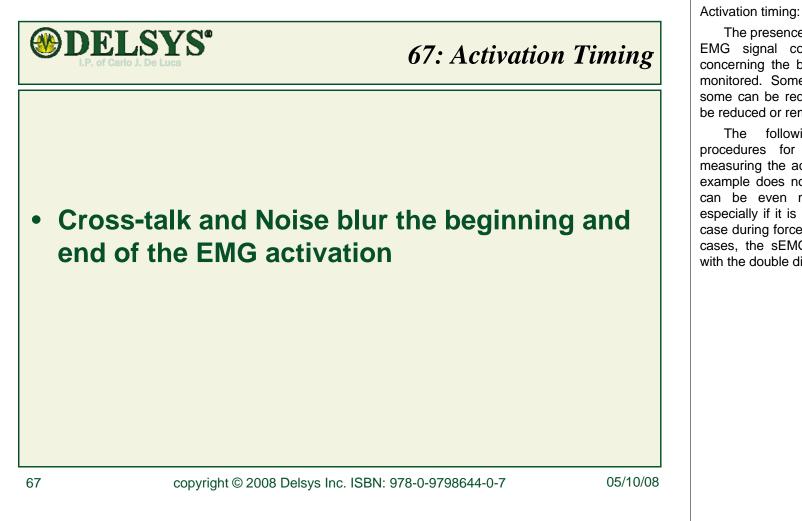




#### Activation Timing:

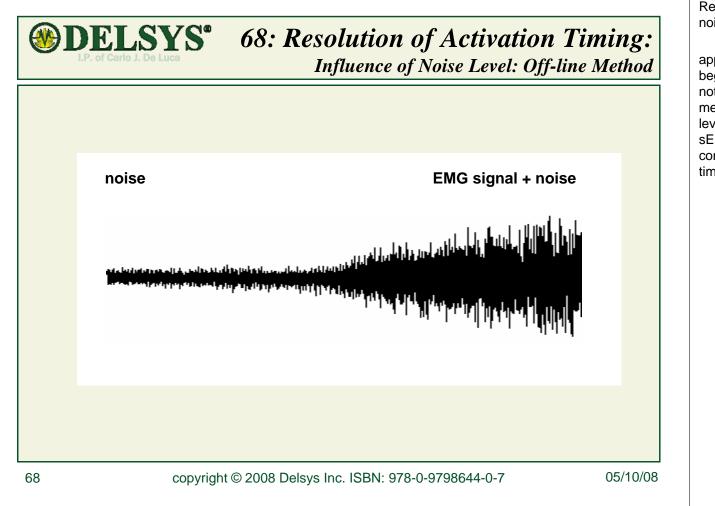
One of the most common use of the sEMG signal is to determine when the muscle contraction begins and ends. That information establishes when muscles are acting as synergists and/or antagonists. In the example above, the top trace has a red line that indicates when the contraction begins and ends. The red shaded region indicates when the muscle in the top trace is co-activated with the muscle in the bottom trace.

The designation of the begin and end time is made difficult by the presence of noise and cross-talk. Of the two, the more damaging is the cross-talk. The noise is mostly constant, with the exception of the movement artifact, whereas the cross-talk varies in a fashion similar to the sEMG signal of interest.



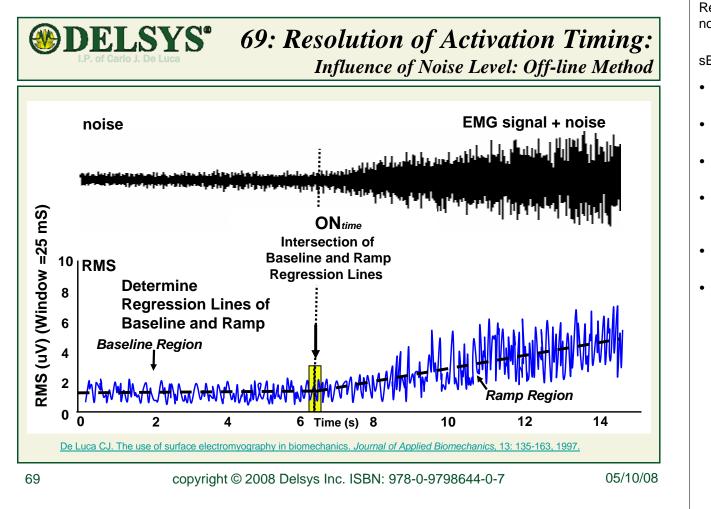
The presence of cross-talk and noise in the EMG signal contaminates the information concerning the behavior of the muscle being monitored. Some of the noise is inevitable, some can be reduced, and the cross-talk can be reduced or removed.

The following slides will describe procedures for dealing with noise when measuring the activation timing. Note that the example does not deal with cross-talk, which can be even more difficult to deal with, especially if it is not constant as would be the case during force varying contractions. In such cases, the sEMG signal should be recorded with the double differential sensor.



Resolution of activation timing – influence of noise level: off-line method:

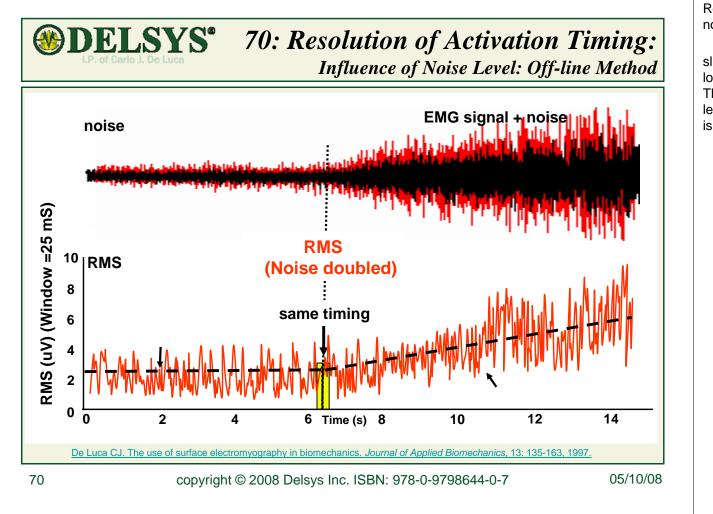
With baseline noise and the often erratic appearance of the EMG signal, finding the beginning of the signal, or activation timing, is not a trivial matter. Here we will see one method which is independent of the noise level. This is a sample of baseline noise and an sEMG signal at the beginning of a weak contraction, for which we will find the activation timing.



Resolution of activation timing – influence of noise level: off-line method:

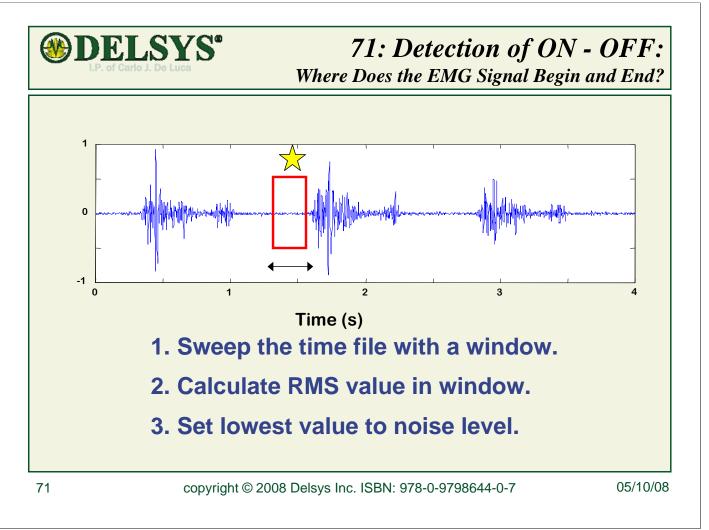
This method of determining where the sEMG signal begins is as follows:

- Find a segment of the signal that has a constant lowest level value.
- Calculate the RMS value with a window of 50 ms or less.
- Calculate the regression line for this segment.
- Follow the signal until it begins to increase, and calculate the regression for the segment with the increased signal.
- The point where the regression lines meet is the ON time.
- Perform reverse calculation for finding the OFF time.



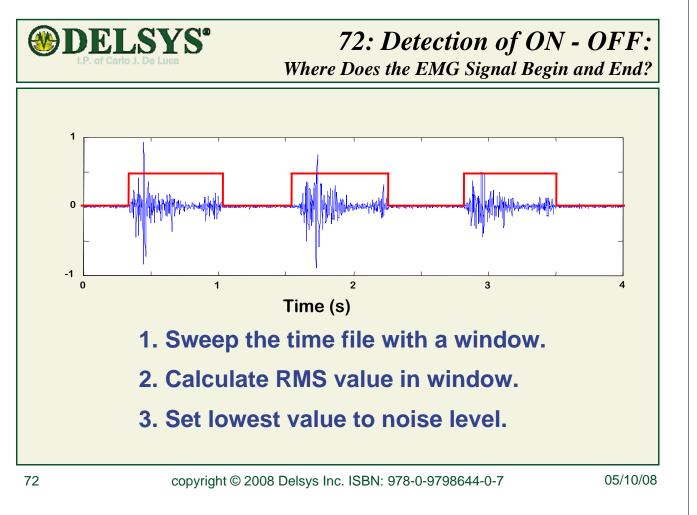
Resolution of activation timing – influence of noise level: off-line method:

The procedure described in the previous slide is independent of the noise amplitude, as long as it is lower that that of the sEMG signal. This can be seen in this slide, where the noise level is doubled, but the activation timing found is the same.



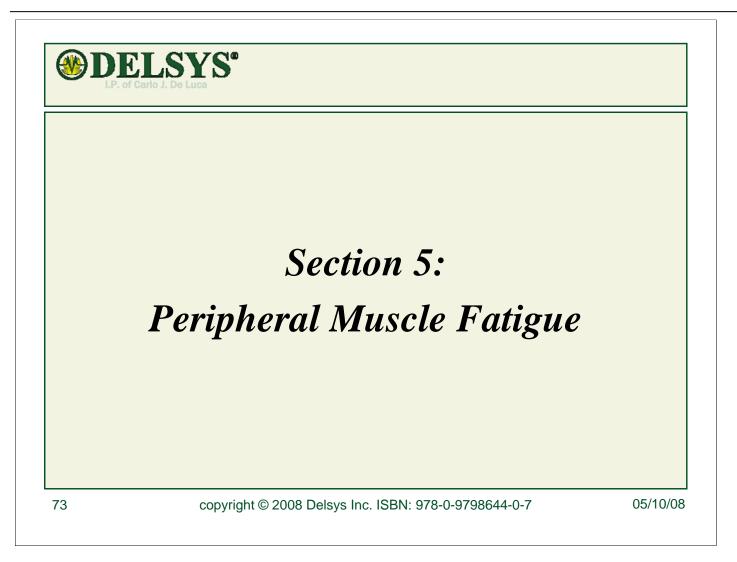
Detection of ON – OFF: where does the EMG signal begin and end?:

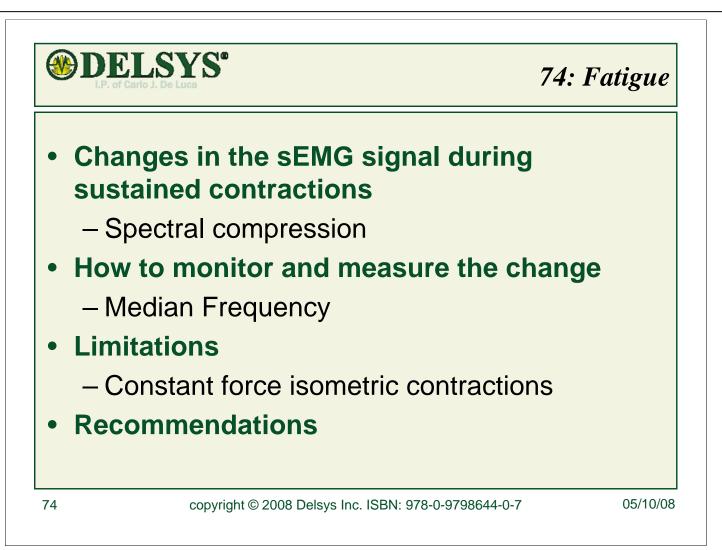
This is an alternative method of resolving baseline noise from the signal of interest. Begin with a window size of 50 ms. Gradually expand the window size as necessary to obtain consistent and realistic results. The lowest value of RMS calculated in the window is set to the noise level. The advantage of this method is that it does not require regression calculations and in some cases may be performed in real time.

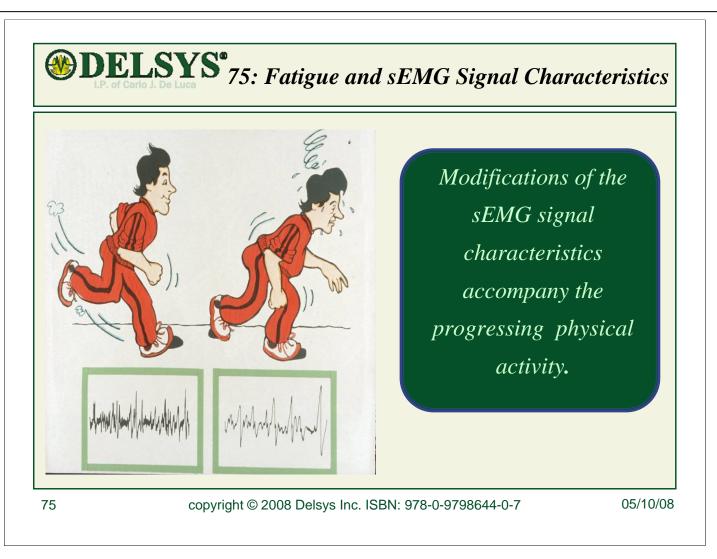


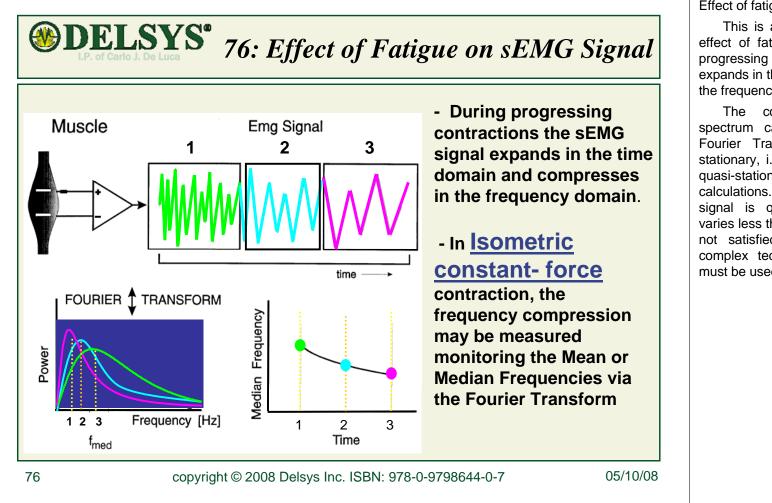
Detection of ON – OFF: where does the EMG signal begin and end?:

Anything with an RMS greater than that of the noise is considered to be part of the signal of interest, shown on this slide in the raised red rectangles.





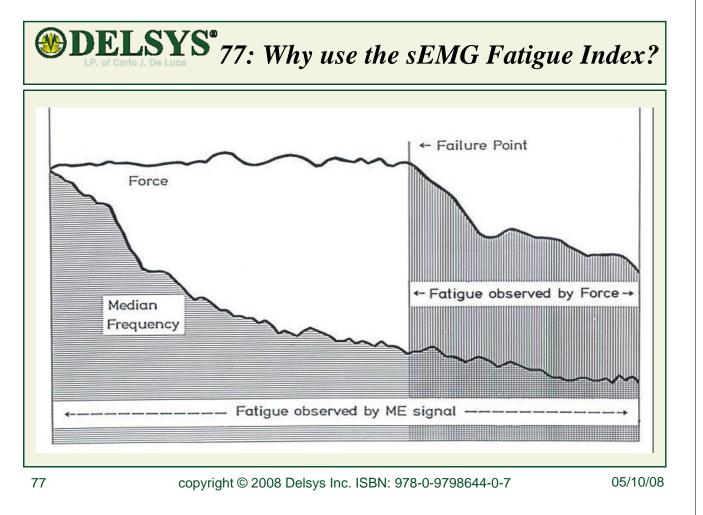




Effect of fatigue on sEMG signal:

This is a schematic representation of the effect of fatigue on the sEMG signal during progressing physical activity. The signal expands in the time domain and compresses in the frequency domain.

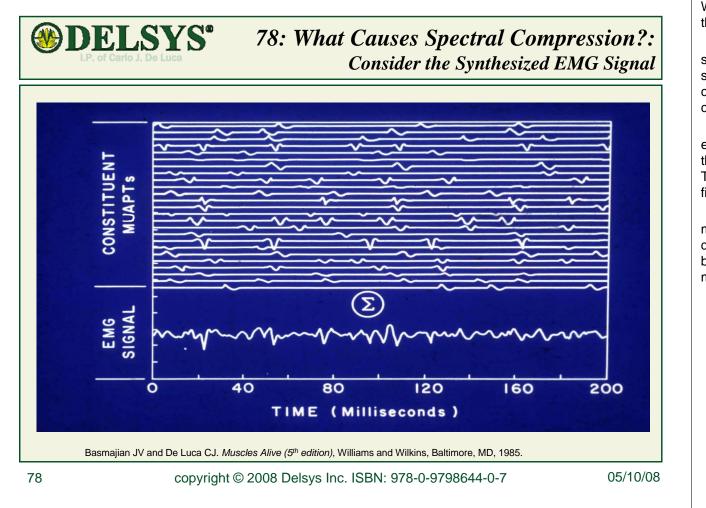
The compression of the frequency spectrum can be monitored by using the Fourier Transform if the sEMG signal is stationary, i.e., it is time invariant. In practice quasi-stationary is sufficient for useful calculations. As a practical rule of thumb, the signal is quasi-stationary if the amplitude varies less than 2% over 2 s. If this condition is not satisfied, than a more mathematically complex technique, time-frequency analysis, must be used.



Why use the sEMG fatigue index?:

The slide shows a cartoon of voluntary constant-force contraction that is sustained up to a failure point, where the desired force level cannot be maintained and it decreases. By normal physiological convention this would be considered the point of fatigue. This convention is inconsistent with that used in physics and engineering. In those disciplines fatigue is a time dependent process that leads to a failure point. For example consider the crystalline structure of the steel alloy used in I-beams of a bridge. As time passes the crystalline structure is altered loosing binding strength. At some point, the I-beam fails and fractures.

The time course of the median frequency of the sEMG signal presents a behavior that is consistent with the notion of fatigue used in physical sciences and engineering.

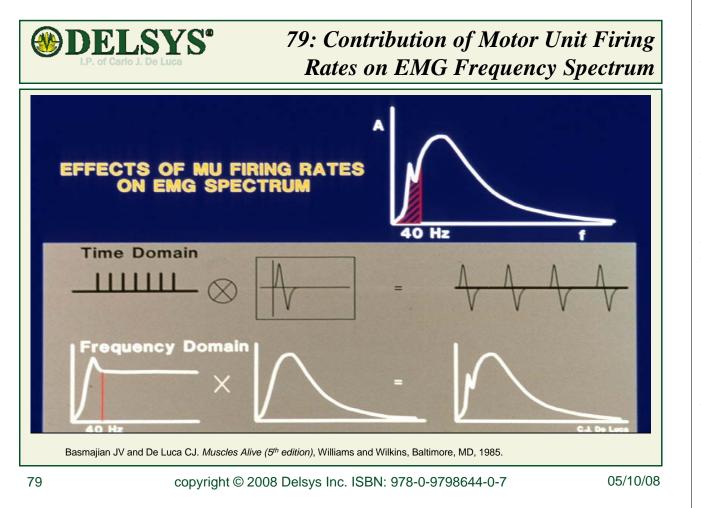


What causes spectral compression? Consider the synthesized EMG signal:

It is useful to review the construct of the sEMG signal before progressing to the next slides which discuss the spectral characteristics of the signal during sustained contractions (fatigue).

Note that the sEMG signal can be effectively modeled as a linear superposition of the individual Motor Unit Action Potential Trains which are generated by the repetitive firings of motor units.

In the following slides we will show that the modifications which occur to the sEMG signal during fatigue are related to physiological and biochemical factors that transpire within the muscle.



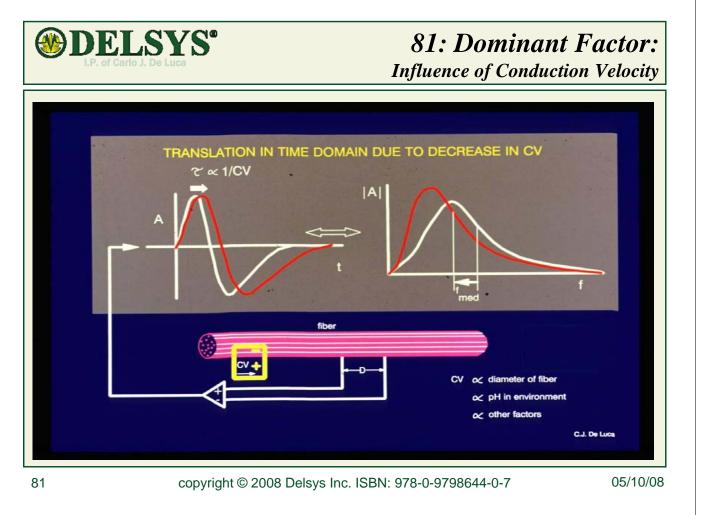
Contribution of motor unit firing rates on EMG frequency spectrum:

The shape of the frequency spectrum of the Motor Unit Action Potential Train is determined almost entirely by the shape of the motor unit action potential. The firing rate has minor influence in the frequency range below 40 Hz (shown in red in the top plot). Even in this range the influence is not systematic, as the location of the frequency corresponding to the average value of the firing rate wobbles because the firing intervals of the motor unit is a Quasi-random process.

Thus, the compression of the sEMG frequency spectrum during fatigue is related to the modifications that occur to the motor unit action potential shape.

The Motor unit Action Potential Train shown as a time series of biphasic pulses can be represented mathematically by a convolution of the train of impulses (Dirac Delta functions) and a pulse representing the Action Potential. Below these time domain representations are the corresponding Fourier Transforms. Note that the transform of the impulse train is flat except for the range below 30 to 40 Hz.

<b>DELSYS</b> <sup>®</sup> L.P. of Carlo J. De Luca	80: What Causes the Changes in the Shape of the MUAP?			
• Conduction v	velocity of action potential			
	ween the origin of the actions of the action scle fiber) and the sensor	on		
80 copyrigh	t © 2008 Delsys Inc. ISBN: 978-0-9798644-0-7	05/10/08		

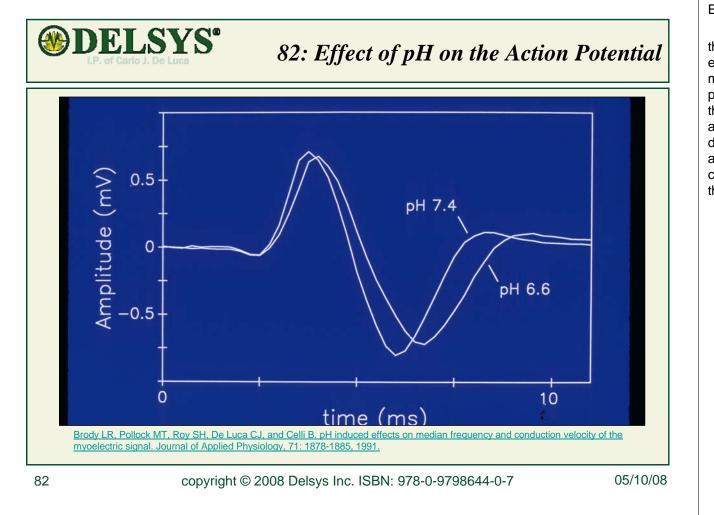


Dominant factor: influence of conduction velocity:

The shape of the action potential can be modified by changing the conduction velocity (CV) along the muscle fibers as shown in the diagram. Consider a single differential sensor with inter-electrode spacing "D". As the depolarization moves near and past the sensor, the detected action potential has a time duration that is a function of the inter-electrode spacing "D", the CV, the voltage decrement function of the depolarization zone (shown as a yellow square) as it radiates through space, and the charge distribution along the depolarization zone.

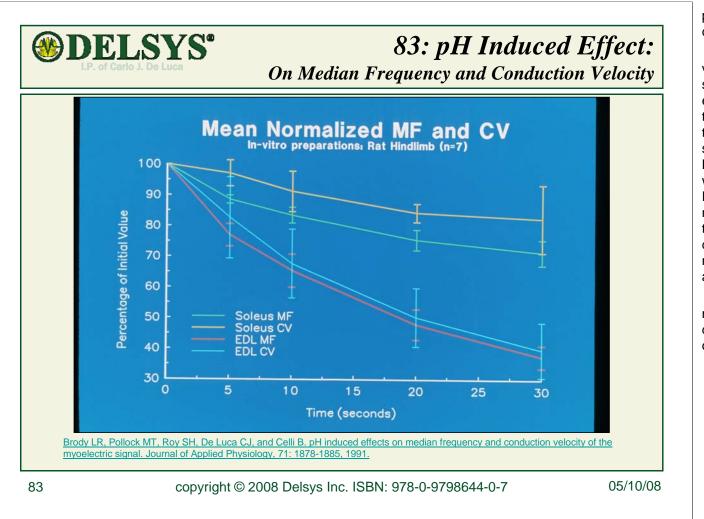
When the depolarization zone is approximately in the middle of the distance between the electrodes the action potential amplitude has a value of zero.

Note that as the CV decreases, the time duration of the action potential increases (red curve) and the frequency spectrum presents an amplitude increase in the lower frequencies and an amplitude decrease in the higher frequencies.



Effect of pH on the action potential:

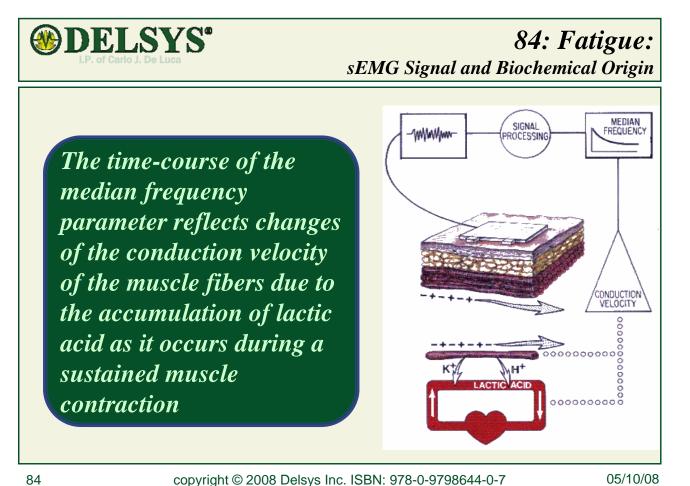
A dominant factor in reducing the speed of the conduction velocity is the pH of the extracellular fluid. This figure shows the measured action potential in a nerve-muscle preparation placed in a bath where the pH of the bath could be artificially altered. Note that as the pH is decreased (as would be the case during a sustained contraction due to the accumulation of Lactic acid, a byproduct of the contractile biochemistry), the time duration of the action potential increases.



pH induced effect on median frequency and conduction velocity:

This figure shows that both the conduction velocity and median frequency of the sEMG signal decrease in concert during an electrically-stimulated sustained contraction in two muscles in the rat. The two muscles were the Soleus, which consists of dominantly red, slow twitch fibers, and the Extensor Digitorum Longus (EDL), which consists of dominantly white, fast twitch, highly anaerobic fibers. In the EDL muscle the conduction velocity and median frequency track each other closely throughout the 30s contraction and the decrease is more dramatic than in the Soleus muscle. Note that lactic acid is a byproduct of anaerobic metabolism.

There is a disparity in the decline of the median frequency and the conduction velocity during the first 5s in the soleus muscle, otherwise the two variables track each other.

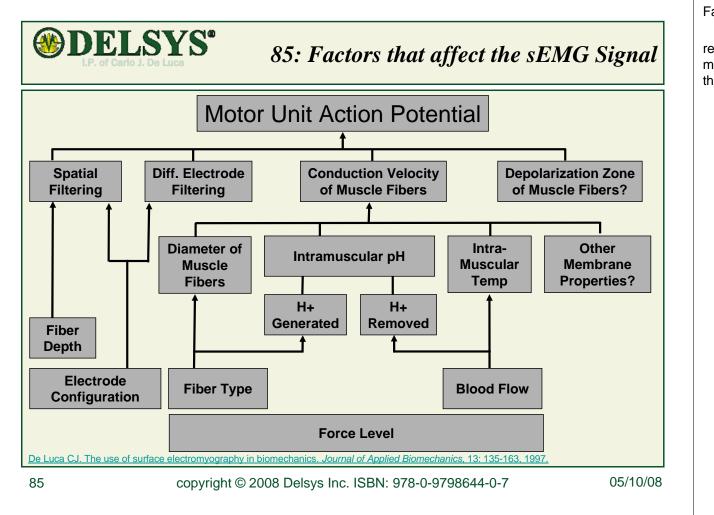


Fatigue - sEMG signal and biochemical origin:

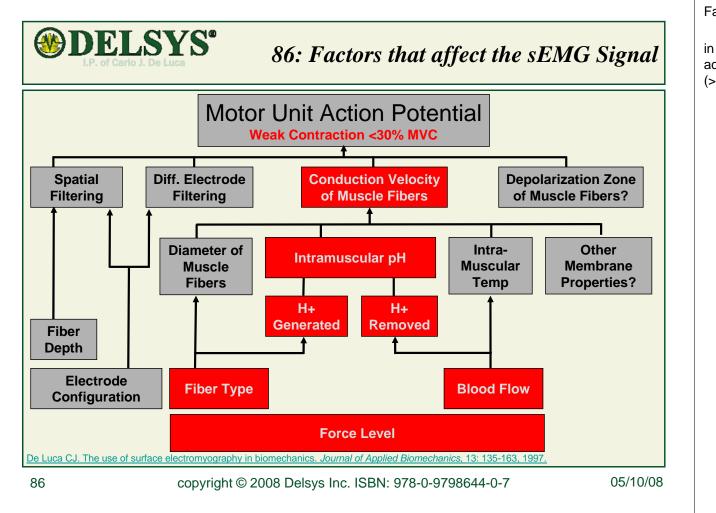
This cartoon shows the likely process that describes the causal relationship between the accumulation of lactic acid in the interstitial fluid and the decrease in the median frequency of the sEMG signal. Note that the accumulation of lactic acid is the difference of the amount that is produced by the contraction of the muscle and the amount that is removed by the blood flow. The blood flow is also a function of the contraction level, because as it increases, the internal pressure in the muscle increases and reduces the volume of the arterioles and veins. In limb muscles, the arterioles collapse at approximately 30% MVC. At greater contraction levels, almost all the lactic acid produced is trapped in the interstitial fluid.

The increasing lactic acid decreases the pH of the extra-cellular fluid, increasing the H+ concentration which increases the positive charge outside the cell. The K+ inside the cell now needs to move against a stronger repelling electro-chemical gradient slowing down the K+ / Na+ exchange that produces the propagating depolarization, therefore, the conduction velocity decreases. As previously described, the decreasing conduction velocity compresses the spectrum of the sEMG signal towards the lower frequencies.

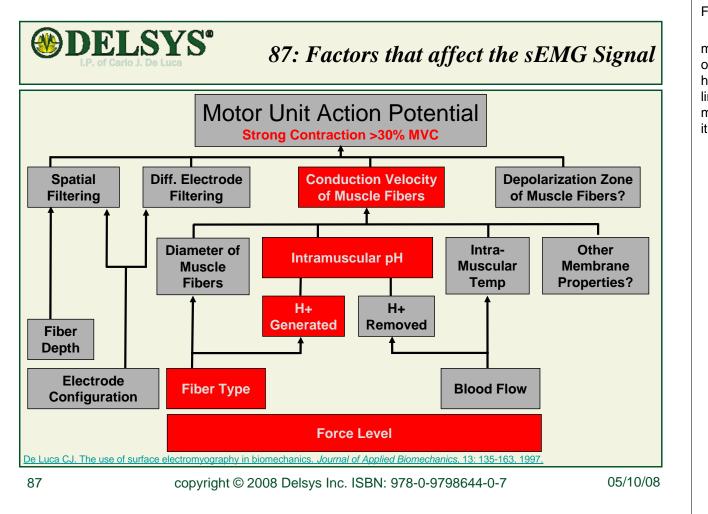
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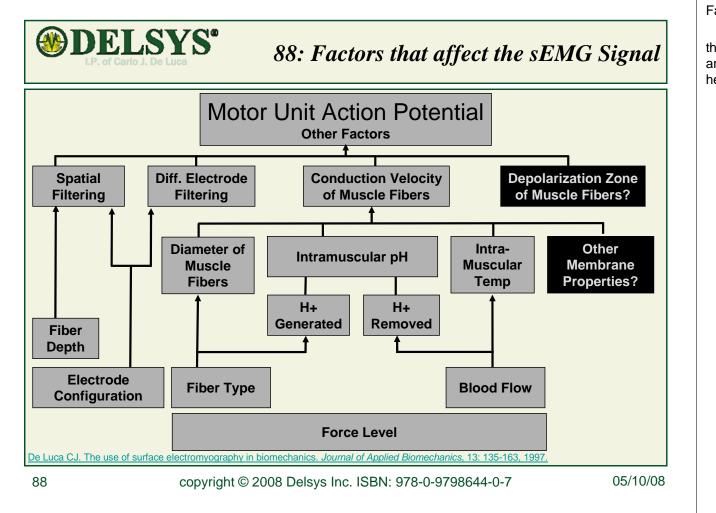
This series of block diagram shows the relationship between force generated by the muscle at different levels and various factors that influence the shape of the action potential.



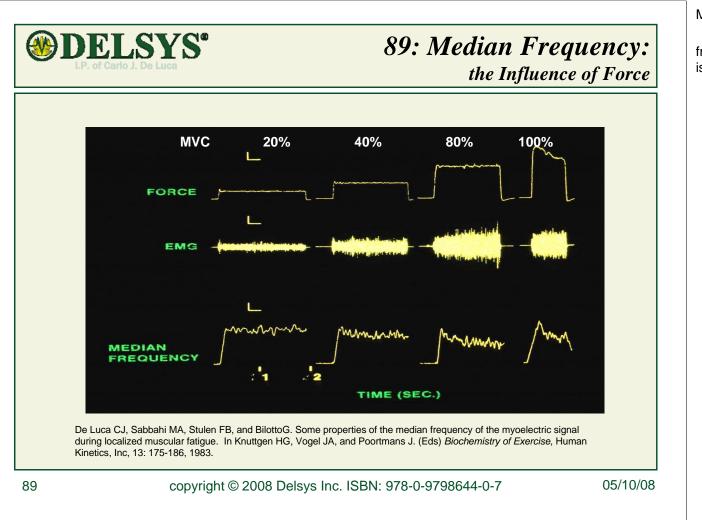
In this slide, factors which take precedence in determining the shape of the motor unit action potential during **weak contractions** (>30% MVC) are highlighted.



In strong contractions (>30% MVC), many of the same factors influence the shape of the motor unit action potential. However, at higher contraction levels, blood vessels in the limbs collapse under pressure from the muscles, so blood flow is no longer a factor, as it is temporarily interrupted.

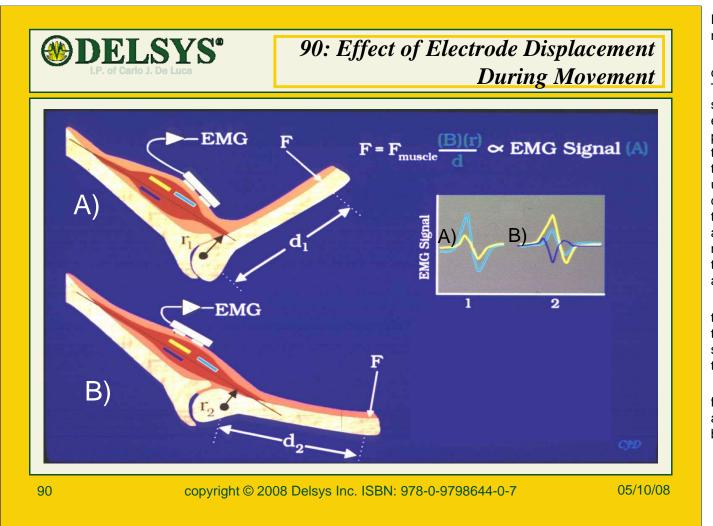


There are still several factors influencing the shape of the motor unit action potential that are not well understood, as highlighted in black here.



Median frequency - the influence of force:

Examples of the decline of the medial frequency at different force levels during isometric constant-force contractions.

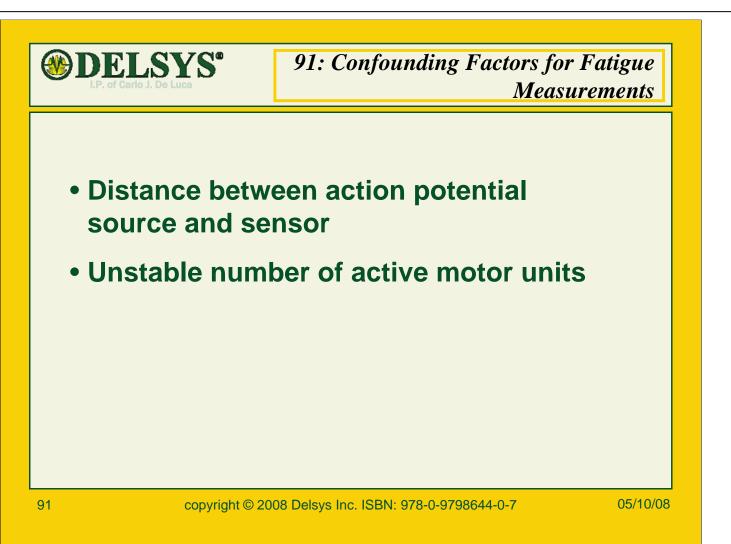


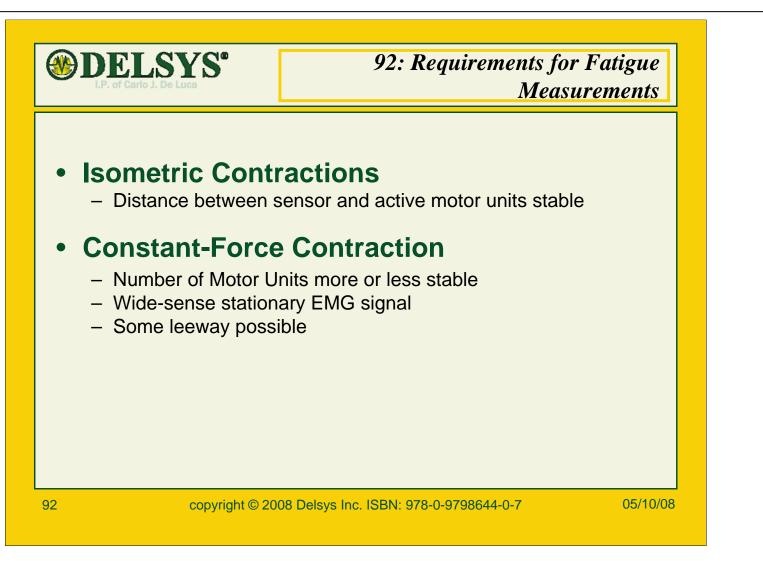
Effect of electrode displacement during movement:

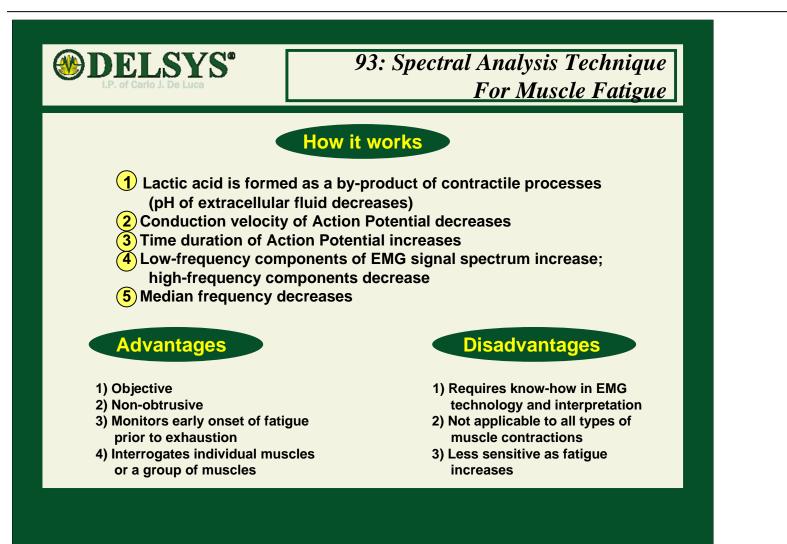
Cautionary Factor -- During a dynamic contraction the length of the muscle changes. The sensor remains affixed in a location on the skin. Thus, the distance between the electrodes and the source of the action potentials changes. There are two concerns: the shape of the action potential changes due to the different spatial filtering and some motor units may be recruited while others may be derecruited. Both these factors are shown in the right quadrant. The dark blue motor unit action potential is recruited in position (B) as it moves closer to the sensor. The shape of all the active (yellow and light blue) motor unit action potentials are modified.

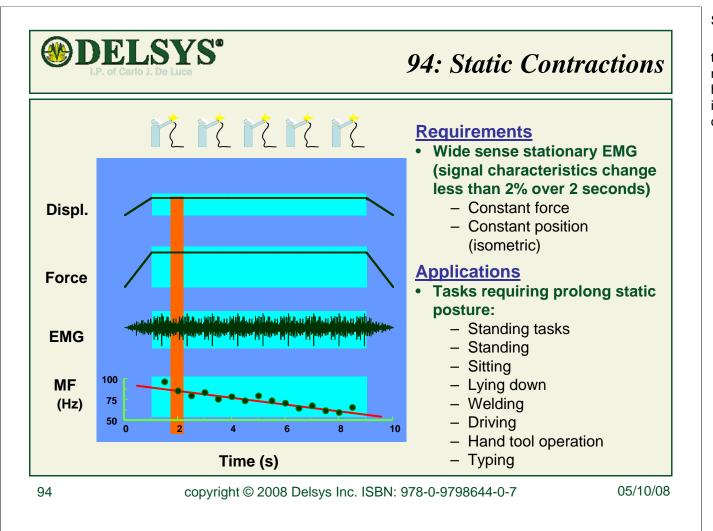
The important point here is that if linear transforms such as the Fourier Transform are to be used for calculating the frequency spectrum of the sEMG signal the contraction is to remain isometric.

There are other techniques such as timefrequency analysis that can cope with some amount of movement, but that discussion is beyond the scope of this practicum.



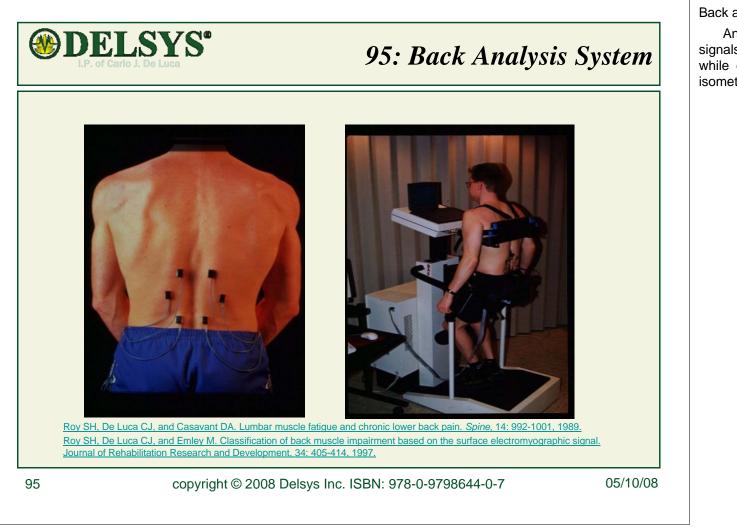






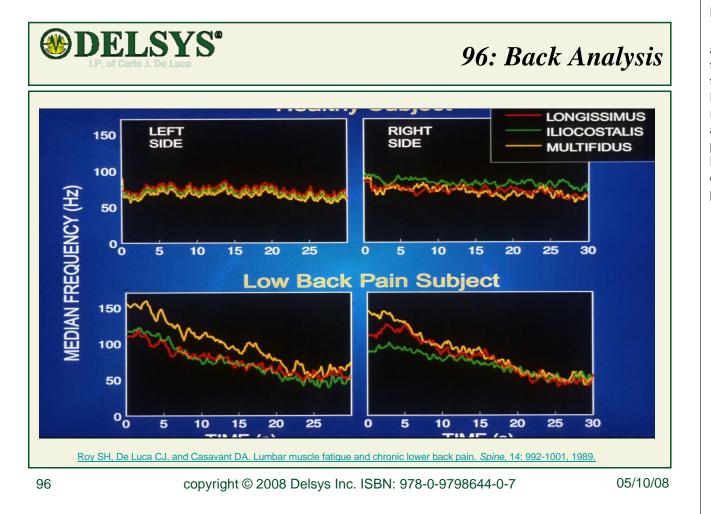
Static contractions:

A cartoon of an appropriate application of the median frequency for measuring peripheral muscle fatigue. In this case the worker is holding a constant load (welding device) in an isometric position. Other examples are listed on the right of the figure.



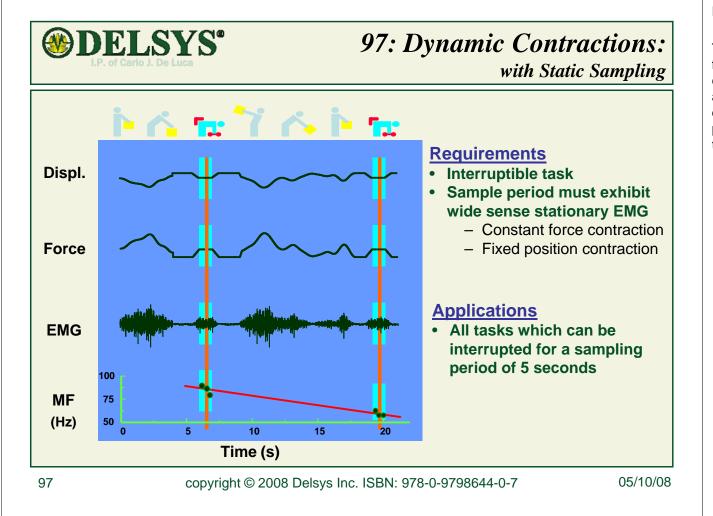
Back analysis system:

An arrangement for obtaining sEMG signals from several muscles in the lower back while constrained in a device that measures isometric contraction of the back.



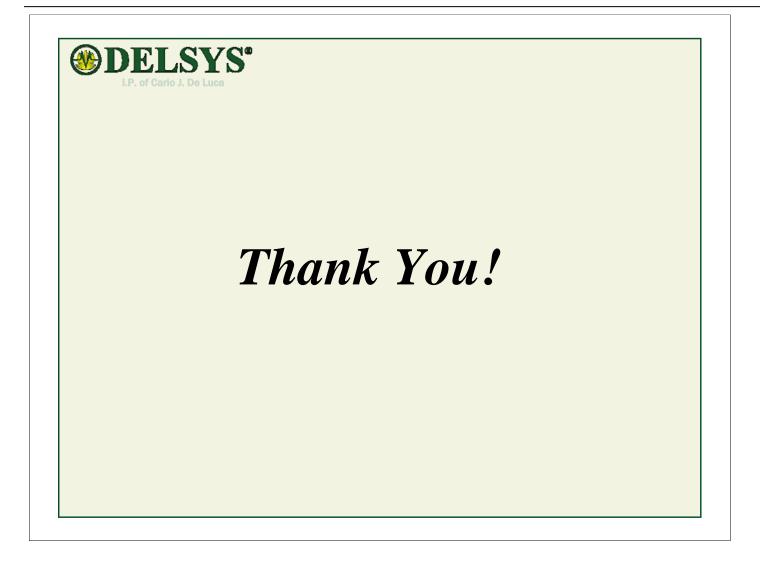
Back analysis:

Results for data obtained from the testing arrangement of the previous figure. The top two panels present the median frequency from the six sensor locations in a healthy individual. Note that the median frequencies remain reasonably constant during a 30 s contraction at 80% MVC. Whereas the same test performed on a patient with diagnosed Low Back Pain revealed median frequencies that decreased dramatically over the same time period.



Dynamic contractions with static sampling:

It has been discussed that the Fourier Transform technique for obtaining the median frequency does not work in dynamic contractions. This cartoon presents an approach that can be used in some repetitive dynamic contractions where the activity can be paused at the same interval during the cycling task as shown at the top of the slide.



### Sensor Related Factors and Fidelity of the sEMG Signal<sup>©</sup>

#### ISBN: 978-0-9798644-1-4 Carlo J De Luca 29 July, 2007

Electrode – The metal surface of the sensor which makes electrical contact with the skin.

<u>Sensor</u> – The unit that contains the electrodes and the electronic circuitry for differential amplification of the EMG signal and reduces the contribution of various noise sources.

<u>Noise</u> – Those electrical signals which are detected by the electrodes and the remainder of the sensor, but do not originate in the muscle below the sensor.

The following table outlines the relationship between sensor design, user preparation, sEMG signal, and various noise sources. Note that the sensor application and the skin preparation play important parts in detecting an sEMG signal of high fidelity. The dominant factor in the User Preparation is the location on the muscle where the sensor is attached. The proper sensor location can enhance the amplitude of the sEMG signal and reduce the crosstalk much more dramatically than the design of the sensor. Thus, the signal fidelity is in large part influenced by proper choice of sensor location – a decision that is left to the user.

Key to table - independent variable -- Sensor Design and User Preparation dependent variable -- Signal and Noise Source

dependent variable increases as the independent variable increases



dependent variable decreases as the independent variable increases

The dependent variable either increases or decreases

(The larger arrows indicate a more dominant factor.) (Green indicates a favorable occurrence, red indicates an unfavorable occurrence.)

ACTIVE DIFFERENTIAL	SIGNAL	NOISE SOURCES				
SENSOR		Cross-	Movement	Baseline	Line radiation	EKG
		Talk	Artifact		(50, 60 Hz)	
Sensor Design						
Inter-electrode spacing						
Electrode area				▼		
Electronics quality				•	•	
Sensor construction				•	•	
User Preparation						
Location on muscle						
Skin preparation	<b>A</b>					
Liquid electrolyte						
Hydrophilic-gel electrolyte						
Sensor orientation with fibers	▲ ▼					•
Location and size of reference						
electrode						
Proximity to heart						

#### **EXPLANATION**

<u>Inter-electrode spacing</u> – The distance between the electrodes renders an increase in the amplitude [1] of the signal (which is beneficial) as well as an increase in the cross-talk sensitivity (which is detrimental) [unpublished work]. Between the two, it is advisable to reduce the cross-talk sensitivity, because cross-talk is virtually indistinguishable from the EMG signal. With greater inter-electrode spacing, there is a greater chance of detecting the EKG signal if the sensor is placed on the chest or upper back muscles.

Thus, smaller inter-electrode spacing is preferable. Also, the electrodes should have a fixed spacing in order to provide consistent and repeatable measurements of signal amplitude. Delsys uses a spacing fixed at 1.0 cm for this and other reasons.

<u>Electrode area</u> – The larger the area the greater the amplitude of the cross-talk signal. This occurs partially due to the encroachment of the electrodes on the nearby muscles. The baseline noise decreases with increasing electrode area [2].

<u>Electronics quality</u> – Electronics components with higher tolerances generate less baseline noise and are better able to reduce (possibly eliminate) the line radiation noise (50 or 60 Hz) enabling a more accurate performance.

<u>Sensor construction</u> – Features such as surface shielding, component layout, and ground-plane geometry can reduce the baseline noise and the line radiation noise.

Location on muscle – If the sensor is placed:

1) Near the innervation zone – the amplitude of the sEMG signal will decrease because cancellation occurs among the action potentials which propagate in opposite directions. The bandwidth of the signal will increase because the subtraction of action potentials moving in opposite directions yields residuals that have sharper transition in the time course of the signal.

In most large muscles, the innervation zones are located at the perimeter of the muscle or near the tendon- muscle interface [3].

2) Near the tendon – The amplitude of the sEMG signal will be relatively lower because the number of muscle fibers and the diameter of the muscle fibers are reduced in this region. Consequently the there are fewer action potentials that contribute to the sEMG signal and those have lower amplitudes.

3) Near the perimeter of the muscle – In most muscles, especially in the larger muscles, the amplitude of the sEMG signal will be relatively lower because there are fewer fibers in this region. Sensors located in this region detect an increased amount of cross-talk from adjacent muscles when they are active, which is likely to be so during most contractions.

**PLACE sensor in the MIDDLE of the muscle surface** – This location lies between the innervation zones (near the perimeter of the muscle) and the tendon- muscle interface. It satisfies the above considerations in most large muscles. In smaller muscles, such as those in the hand, there is no choice as to where to locate the sensor.

<u>Skin preparation</u> – The oils and debris that normally accumulate on the skin must be removed in order for the ionic exchange to occur effectively between the salts in the skin and the metal of the electrode. Removal of the oils and debris decreases the impedance of the electrical contact and increases the effectiveness of the sensor which renders increased sEMG signal amplitude, a decreased baseline noise, and, at times, a reduced line radiation noise.

<u>Liquid electrolyte</u> – Delsys EMG sensors do not normally require an electrolyte to make proper electrical contact with the skin when the skin is cleaned properly. These are referred to as "dry' sensors. They were first introduced by Delsys personnel in 1979 [4]. If the signal quality requires improvement, then a liquid electrolyte should be applied to the surface of the electrodes only. Be very careful not to apply electrolyte on the skin as this would cause an electrical short between the two electrodes and would worsen the signal quality.

<u>Hydrophilic-gel electrolytes</u> – Do not use hydrophilic gel electrolyte if it is likely that a force impulse will be transmitted through the limb to which the senor is attached, as it will enable the occurrence of movement artifact [5]. The viscosity of the hydrophilic-gel causes relative movement of the electrode with respect to the skin, both in the normal (perpendicular) as well as the shear (parallel) direction.

<u>Sensor orientation with fibers</u> – The orientation of the sensor, hence the electrodes, with respect to the direction of the muscle fibers can influence the amplitude of the sEMG signal. The greatest amplitude is obtained when the electrode is perpendicular to the fibers. Also, changing the sensor orientation with respect to the heart will reduce the EKG signal, if one is detected. The sensor is a differential amplifier, thus if both electrodes are arranged so that they are equidistant in the EKG current path the EKG signal will be common mode (similar in amplitude and phase at both electrodes) and it will be removed. If the electrodes are placed along the path of the EKG current, then a differential voltage will be amplified and the EKG signal may be detected.

<u>Location and size of reference electrode</u> – It is advisable to place the reference electrode as far away from the sEMG sensor as is convenient, and not near sources of line radiation such as power cables or lights. Clean the skin with alcohol. Use large (4 to 5 cm) electrodes with strong adhesives that make an effective electrical contact. Placing the reference electrode close to the sensor may disturb the sEMG signal, especially if multiple sensors are attached to the body. An effective reference electrode contact is important. Choose a location that decreases noise interference and prepare the skin accordingly.

<u>Proximity to heart</u> – When recording sEMG signals from muscles in the chest and upper back it is possible to detect the unwanted EKG signal while detecting the sEMG signal. This interference can be reduced and at times eliminated by using sensors with small inter-electrode spacing and by rotating the alignment of the sensor with respect to the heart.

#### Reference

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## **RECOMMENDED PRACTICE** (in order of importance)

- 1) Use a sensor with a 1 cm inter-electrode spacing.
- 2) Place sensor in the middle of the muscle surface.
- 3) Orient the electrodes along the length of the muscle fibers. If using the Delsys sensors, align the arrow along the muscle fibers.
- 4) Carefully attach sensor to skin.
  - a. clean skin with 70% Isopropynol alcohol and
  - b. remove excessive hair in most individuals this is not necessary
  - c. use effective adhesive and apply it forcefully
  - d. do not use hydrophilic gel electrolyte if movement artifact is a concern
- 5) Filter signal from 20 to 450 Hz.
- 6) Use high-quality equipment.

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